

Impact of Wide-Base Tires on Pavements – A National Study



5/30/2013



OHIO
UNIVERSITY



Delft
University of
Technology

UC DAVIS
UNIVERSITY OF CALIFORNIA



Agenda

- 08:00-08:30 Introduction/Project Overview
- 08:30-09:15 Tire Contact Stress
- 09:15-10:00 Pavement Modeling (Delft/UIUC)
- 10:00-10:15 **Break**
- 10:15-11:00 Pavement Modeling (Thin & Thick)
- 11:00-12:00 Data Management
- 12:00-13:00 **Lunch**
- 13:00-13:45 Laboratory Testing
- 13:45-15:15 Instrumentation and Field Testing
- 15:15-15:30 **Break**
- 15:30-15:45 Future Plans Discussion
- 15:45-16:15 Technical Committee Discussion
- 16:15-16:45 Final Remarks
- 16:45 **Adjourn**



Project Overview

8:10-8:30am

5/30/2013



Project Overview

- Quantify the impact of **WBT** on **pavement damage** utilizing advanced **theoretical modeling** and validate results using **full-scale testing**
- **Scope:**
 - **Contact stress measurements** of tires (WBT & DTA)
 - **APT** of pavement sections
 - **FEM** modeling of pavement loading
 - Calculation of **pavement damage**



Project Overview

Phase I Tasks

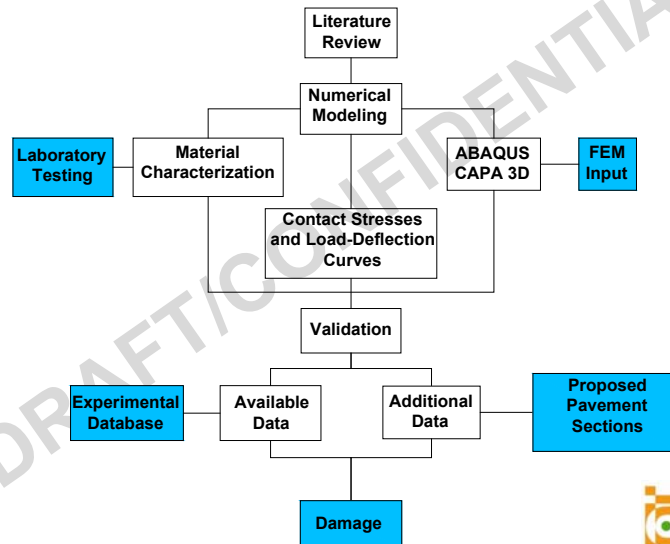
- 1.1. Comprehensive literature review and synthesis on past and current research
- 1.2. Experimental plan and modeling framework
- 1.3. Implementation and marketing plan
- 1.4. Phase I report
- 1.5. Conference call with panel
- 1.6. Presentations to relevant conferences and symposiums

Phase II Tasks

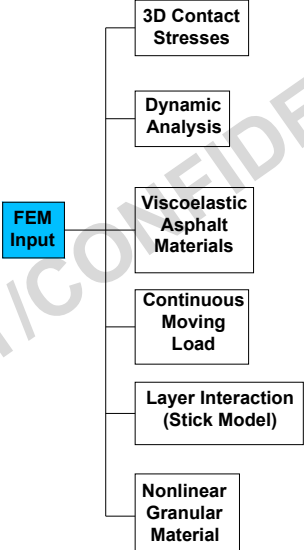
- 2.1. Prepare experimental equipment, test structures, and instrumentation
- 2.2. Conduct experiments (material characterization and APT)
- 2.3. Conduct modeling
- 2.4. Develop of analysis tool
- 2.5. Delivery of draft Phase II report and analysis tool
- 2.6. Present to relevant conferences and symposiums
- 2.7. Prepare article and technical papers



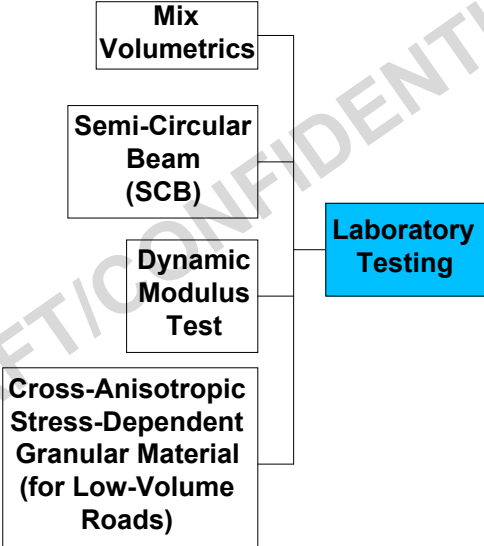
Project Overview

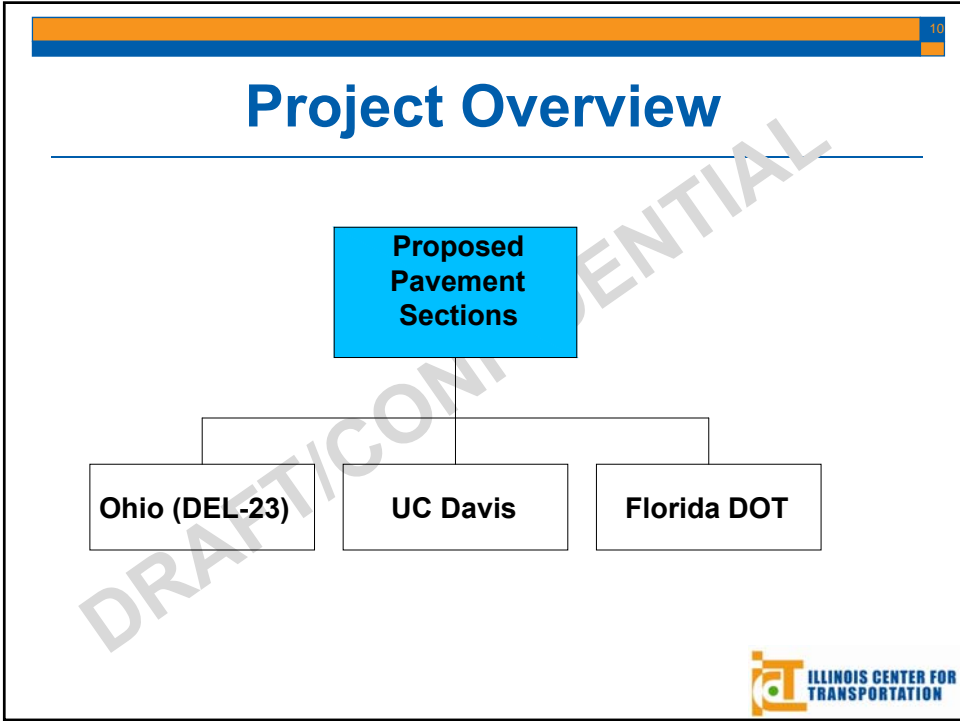
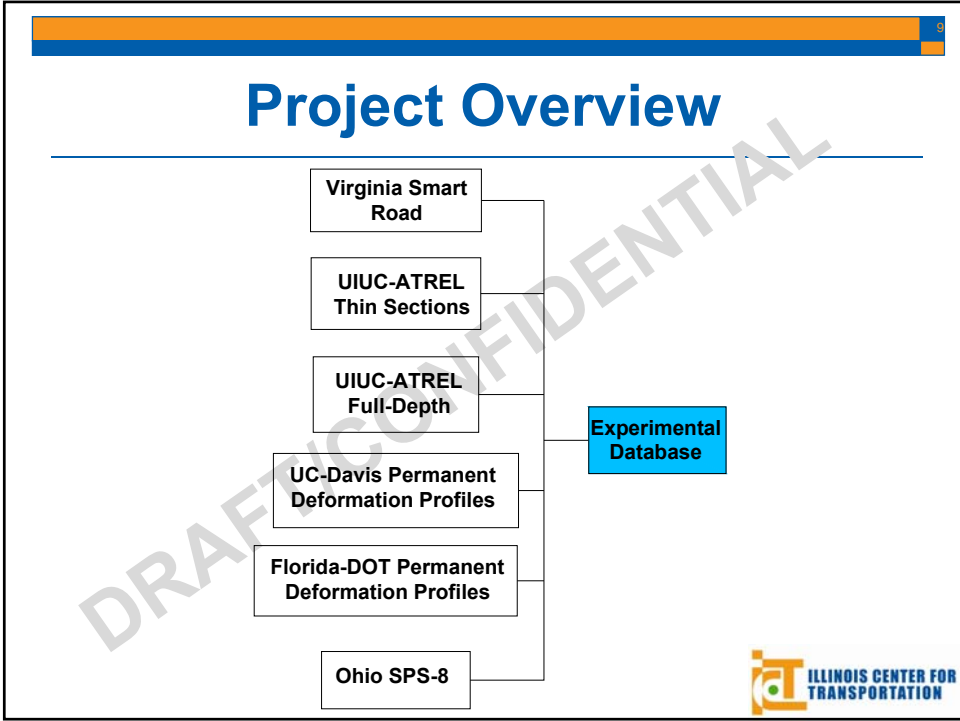


Project Overview

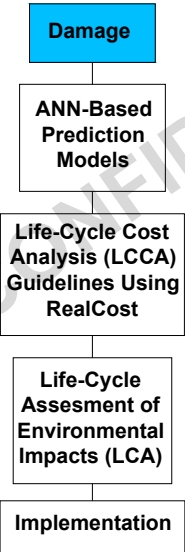


Project Overview





Project Overview



COMMENTS!



Tire Contact Stress

8:30-9:15am

5/30/2013



Outline

- Experimental Program
- Data Processing
- Contact Stress Distributions
- 3D Contact Stresses
- Tire Contact Area
- Maximum Rib Contact Length
- Summary



15

Experimental Program

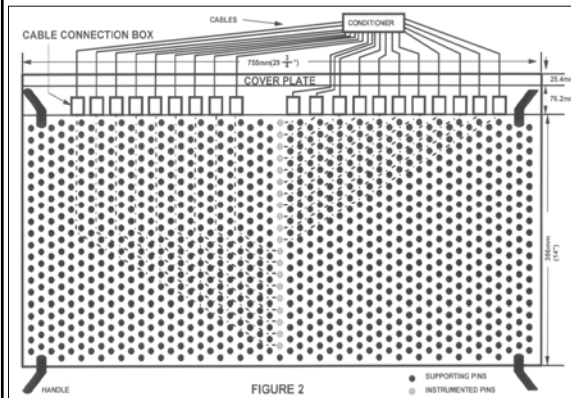
Tire Type	Inflation Pressure (kPa)	Tire Loading (kN)				
		26.6	35.5	44.4	62.2	79.9
NGWB and Dual	552	26.6	35.5	44.4	62.2	79.9
NGWB and Dual	690					
NGWB and Dual	758					
NGWB and Dual	862					
Dual Only	414/758*					
Dual Only	552/758*					

*Differential Tire Inflation Pressure

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Experimental Program: Measuring System

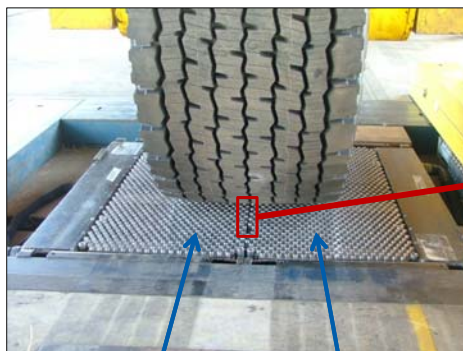


- **Nominal Area:**
840x417 mm
- **1020 Supporting Pins**
- **21 Instrumented Steel Pins**

Single Pad Assembly
(SIM is composed by two Pads)



Experimental Program



Pad Assemblies



Experimental Program

- ❑ Lateral position of tires was fixed
- ❑ Pin measured applied force
- ❑ Average speed: 0.331m/s (1.19km/h)
- ❑ Sampling frequency: 1001hz
- ❑ Static imprints of tires obtained
- ❑ Load deflection curves were measured
- ❑ Each load combinations were repeated 10 times; optimum three repetitions were used



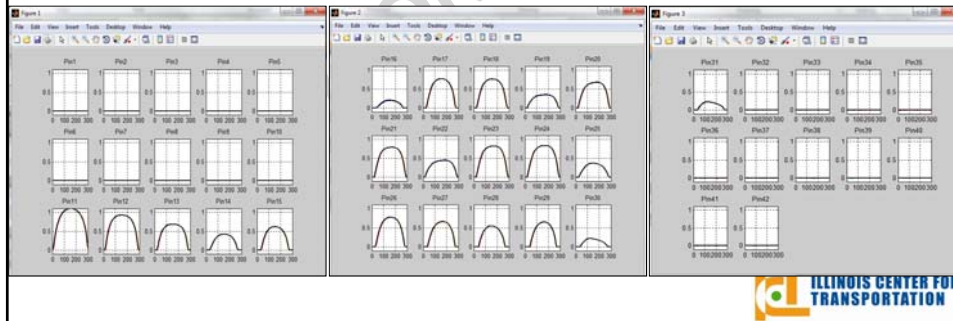
Pin Measurements in txt Format

FILENAME (TXT)	Pressure (kPa)	Pressure (kN)	HVS (m/s)	SPEED (sam/sec)	Hz (KN)	SIM-LOAD Y Direction	Michelin 445/50 R22.5 (XDN2) Data in N Patch Length	X-one Comment
HVS604	862	35.5	0.3405	1001.45	-1	36955	210,124 wideBase Tire	
Counts	0	0	0	0	0	0	0	0
1	0	0	0	0	0	0	0	0
2	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0
19	-1	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0
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25	0	0	0	0	0	0	0	0



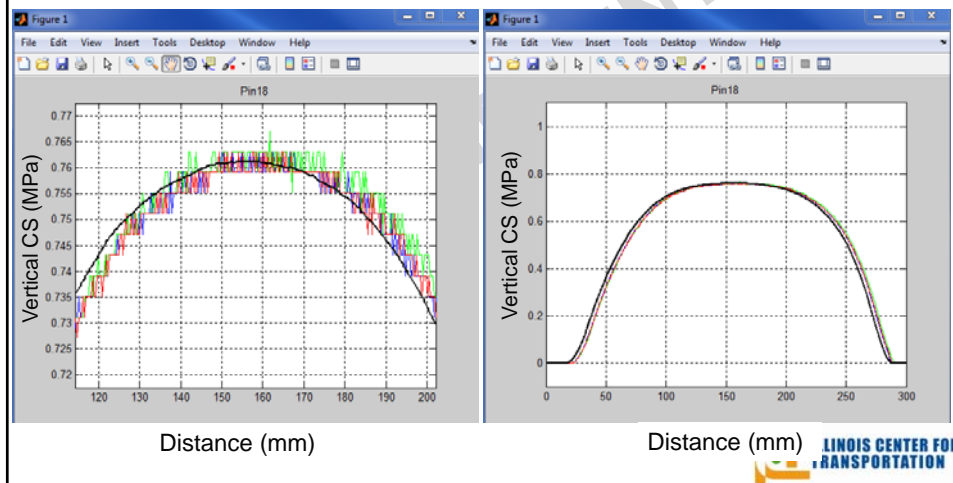
Data Processing

- Script written in **Matlab**:
 - Data filtered using moving average (window size = 20 measurements)
 - Simultaneous observation of three repetitions and filtered data



Data Processing

- Filtering data using moving average



Data Processing: Contact Area

- Contact area from footprint (processed in **AutoCAD**)
- Contact length from pin measurements

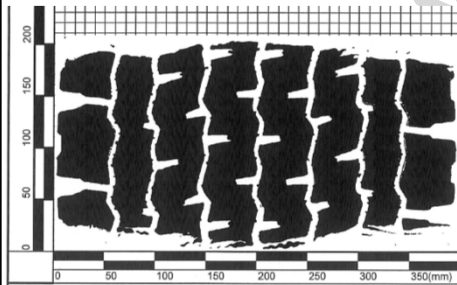


Figure F7
Michelin 445/50 R22.5 (XDN2) X-one

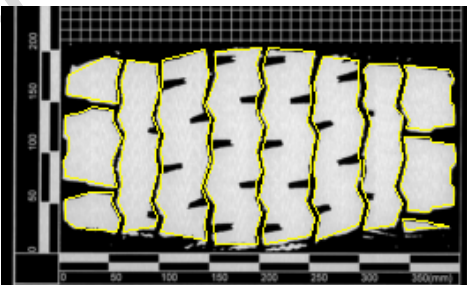
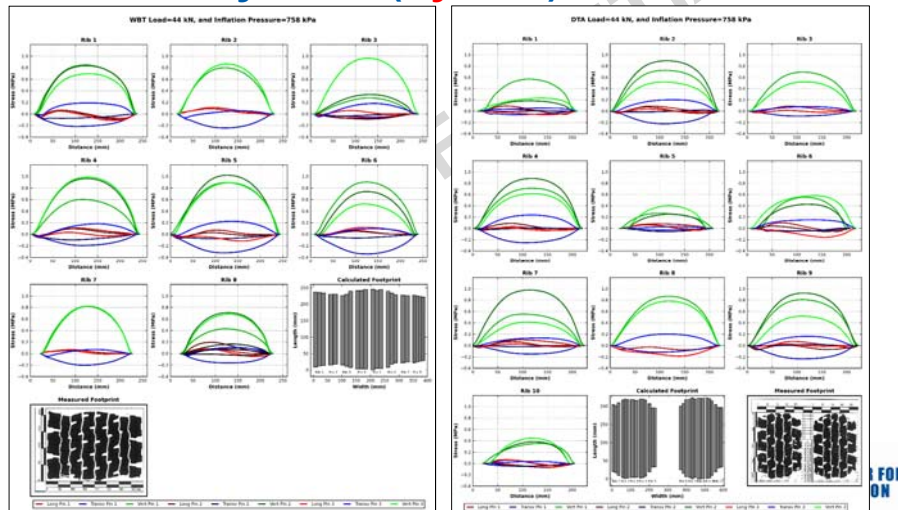


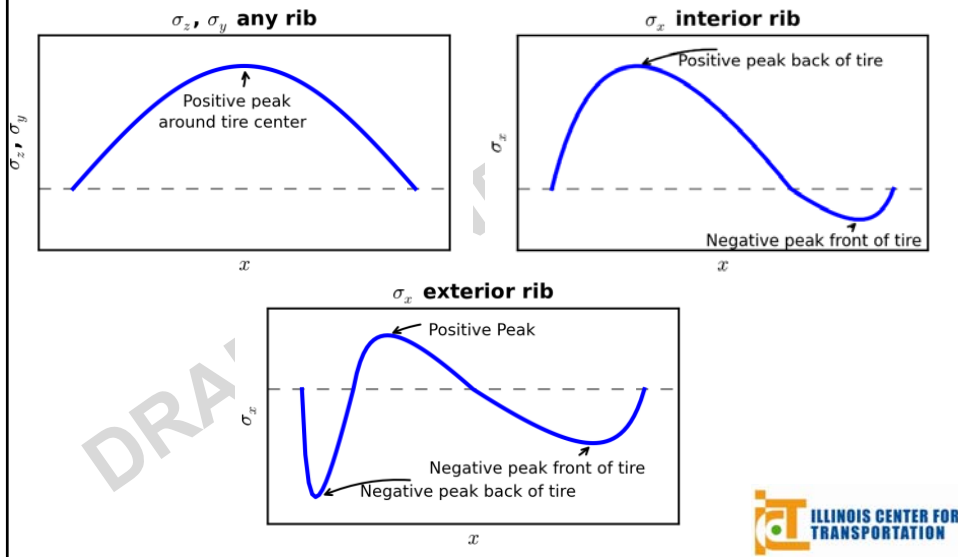
Figure F7
Michelin 445/50 R22.5 (XDN2) X-one

Data Processing

- Summary Plots (**Python**)

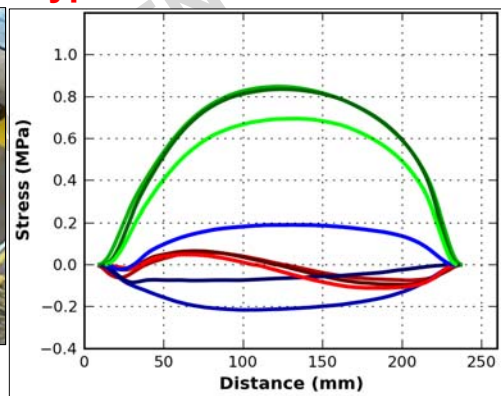
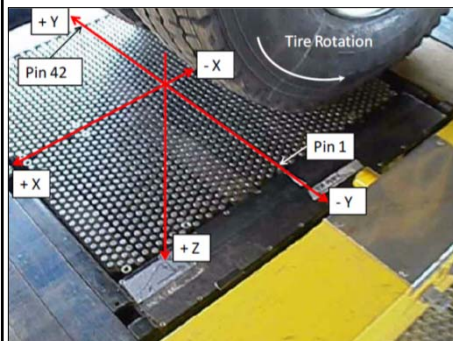


Contact Stress Distributions



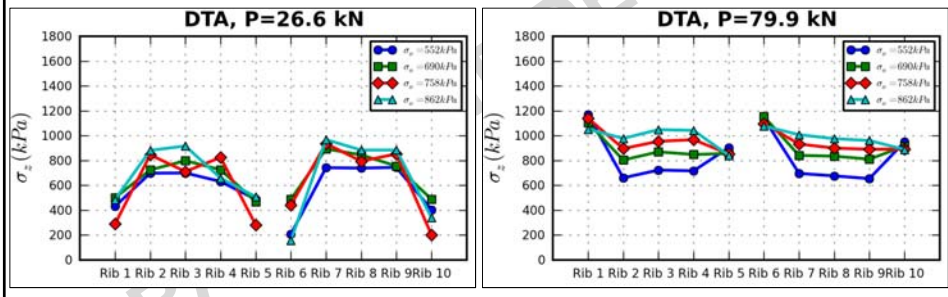
Contact Stress Distributions

Typical Stress Distribution



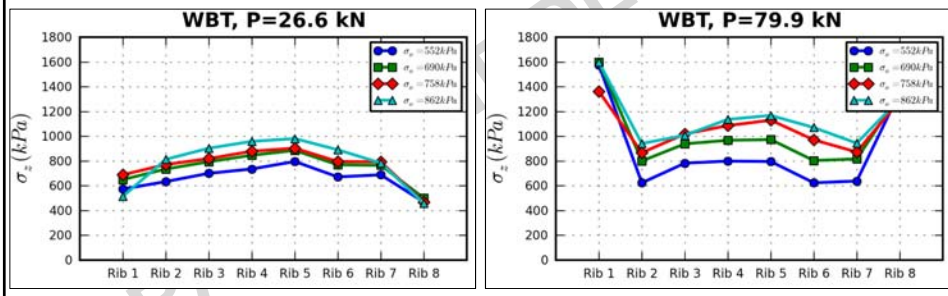
Vertical Contact Stresses

□ “n” and “m” Shape Patterns: **DTA**



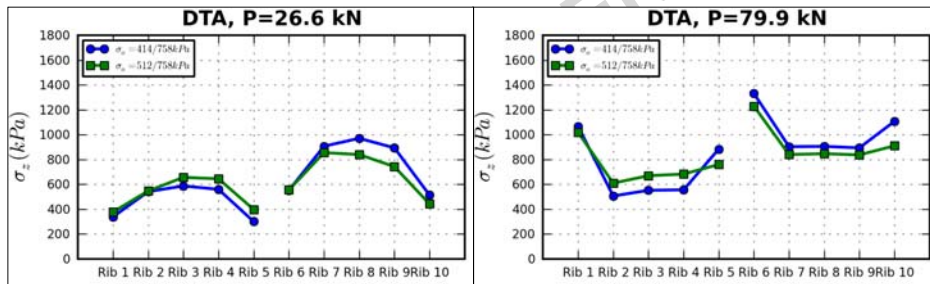
Vertical Contact Stresses

□ “n” and “m” Shape Patterns: **WBT**



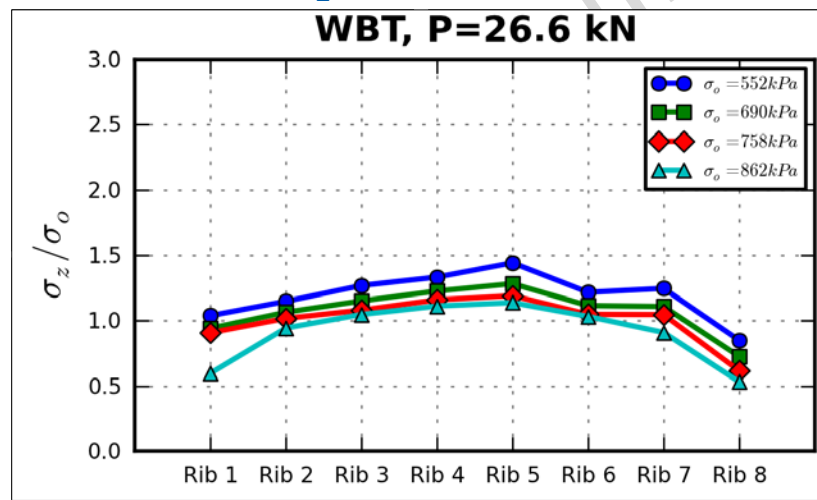
Vertical Contact Stresses

- Effect of σ_o on σ_z for DTA with differential σ_o



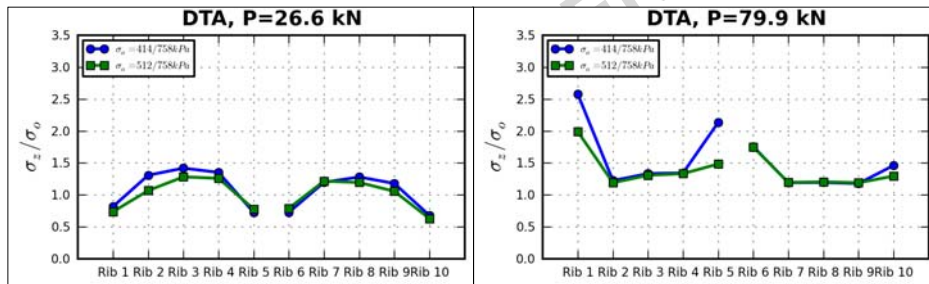
Vertical Contact Stresses

- Normalized σ_z



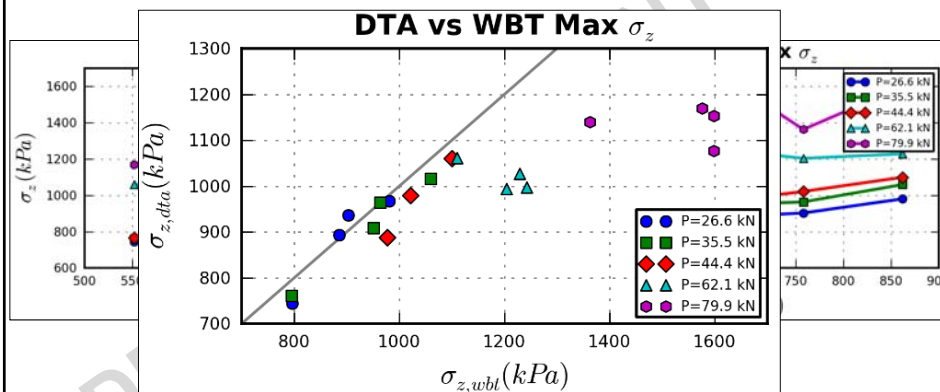
Vertical Contact Stresses

- Normalized σ_z for DTA with differential σ_o



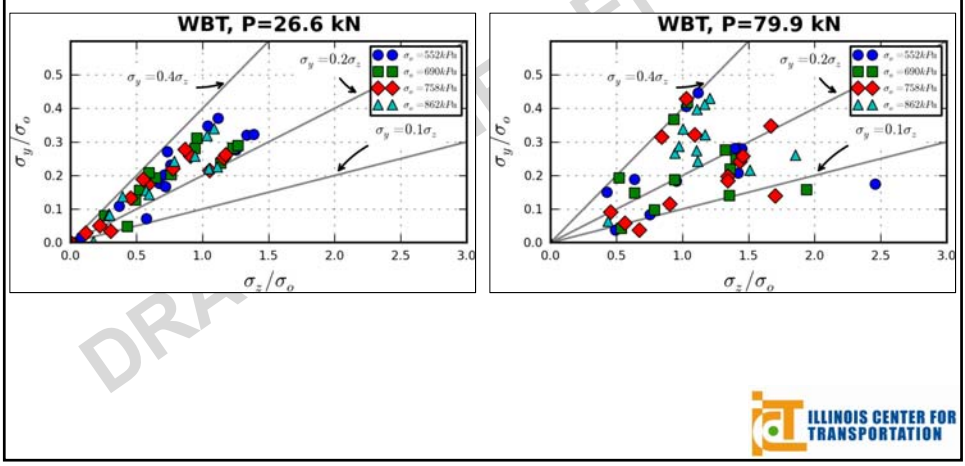
Vertical Contact Stresses

- Maximum σ_z



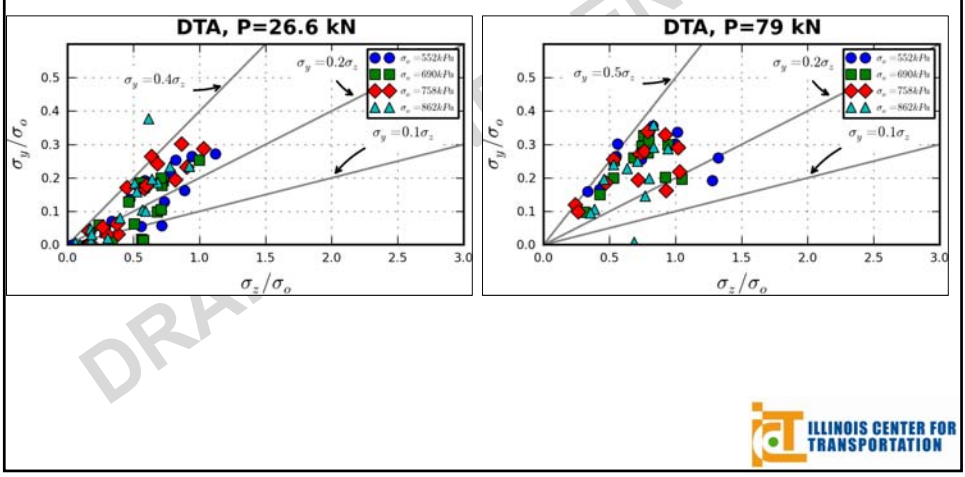
Transverse Contact Stresses

- Maximum σ_y for **WBT**

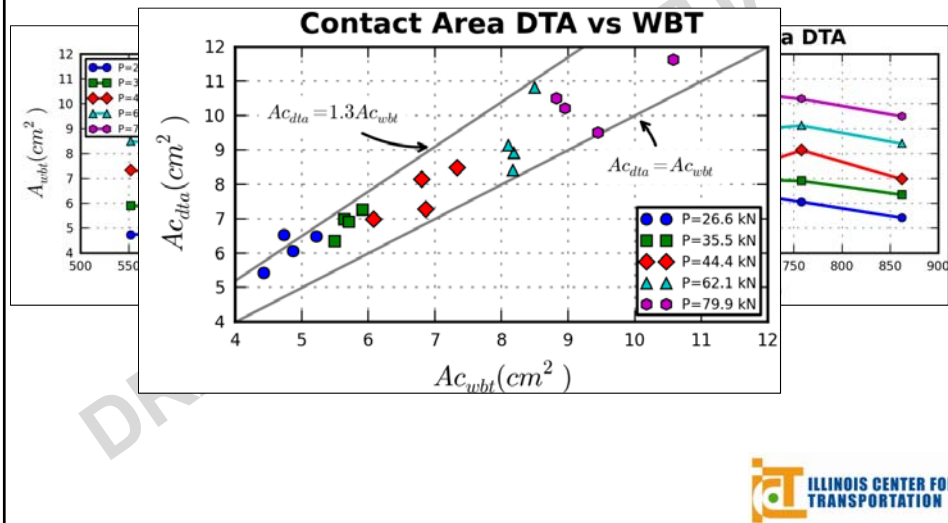


Transverse Contact Stresses

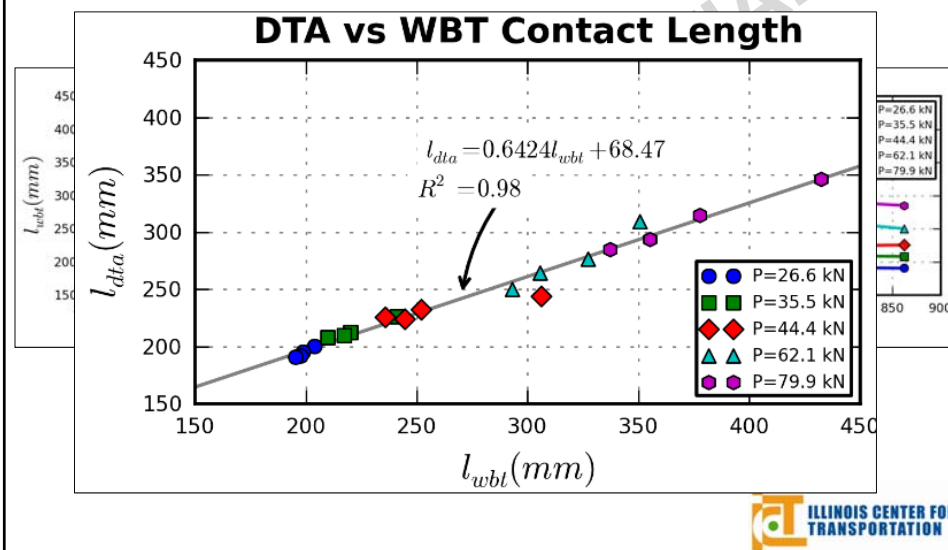
- Maximum σ_y for **DTA**



Contact Area



Maximum Contact Length



Remarks

- Mechanisms of load transfer vary for various tires:
 - Contact **area** may be up to **30% greater** for DTA than WBT
 - Contact **length** may be up to **65% shorter** for DTA than WBT
- Complex **3D contact stresses** are important to determine pavement response
- **Robust analysis** needs to be performed in order to determine the actual **damage** caused by the two tires



Future Plans

- Finalize detailed analysis of DTA and WBT **magnitude** and **distribution** of contact stresses
- Finalize **prediction** of contact stresses using **FEM**




COMMENTS!



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**Pavement Modeling
(Delft/UIUC)
9:15-10:00am**

5/30/2013



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TU Delft Update



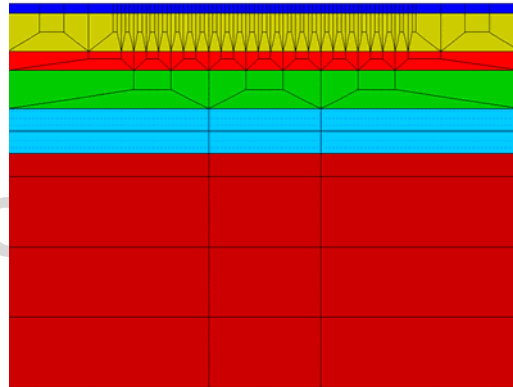
Outline

- ❑ Pavement Structure
- ❑ Mesh Configuration
- ❑ Loading Function
- ❑ Dual and Wide-Base Tires
- ❑ Material Characteristics
- ❑ Analysis Output
- ❑ Completed Tasks
- ❑ Future Works

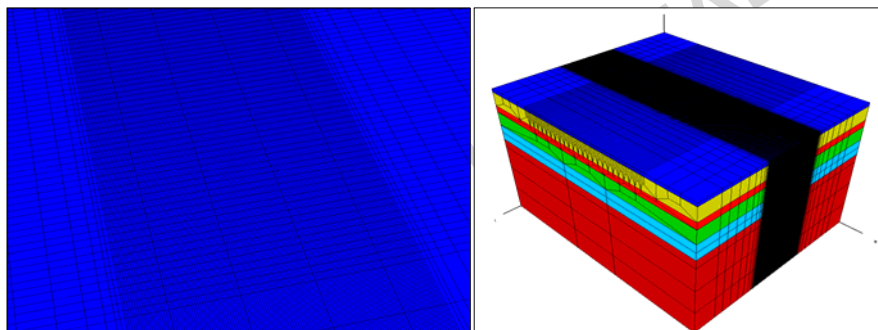


Thick Pavement Structure

Surface Mix (SM-9.5D – 38 mm)
Base Mix (BM-25.0 – 150 mm)
Asphalt-Treated Drainage Layer (OGDL – 75 mm)
21A Cement Stabilized Base Layer (21B – 150 mm)
21B Aggregate Subbase Layer (21B – 175 mm)

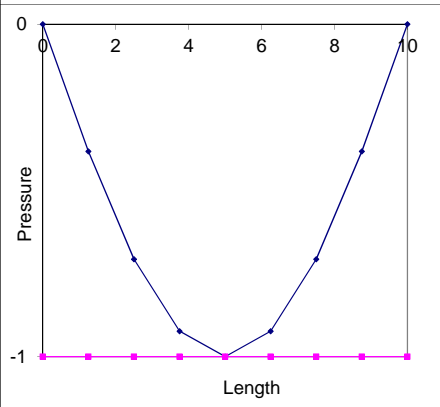


Mesh of Thick Pavement



- Mesh size reduction in the depth direction provides a balance of accuracy directly under the loading area and reduced computational time
- Fine mesh in the transverse direction based on previous research from UIUC

Sinusoidal Loading Function in CAPA-3D



Total force calculated from the closed form solution of the integration of a sine load:

$$F = (p')w = \left(\int_0^{10} \sin\left(\frac{2\pi}{20}x\right) dx \right) \cdot 10 = \left(\frac{10}{\pi} \cos\left(\frac{\pi}{10}x\right) \Big|_{x=0}^{x=10} \right) \cdot 10 =$$

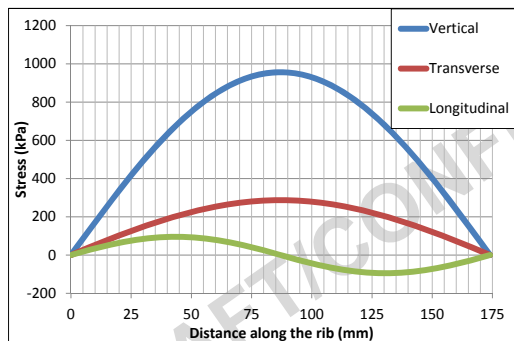
$$= \left(\frac{10}{\pi} (\cos(\pi) - \cos(0)) \right) \cdot 10 = \frac{10}{\pi} (-1 - 1) \cdot 10 = \frac{200}{\pi} = 63.662$$

Sum of reaction forces in CAPA-3D for the same loading as the closed form solution = 63.671

Error of less than 0.01%



General Form of Loading Used



Contact stress distribution in 3D is assumed as follows:

$$\sigma_{ver} = \sigma_{max,ver} \sin\left(\frac{\pi x}{L}\right)$$

$$\sigma_{trans} = 0.3 \sigma_{max,ver} \sin\left(\frac{\pi x}{L}\right)$$

$$\sigma_{long} = 0.1 \sigma_{max,ver} \sin\left(\frac{2\pi x}{L}\right)$$

where,

$\sigma_{max,ver}$ = maximum vertical contact stress in the rib
 L = length of the rib
 x = distance along the rib

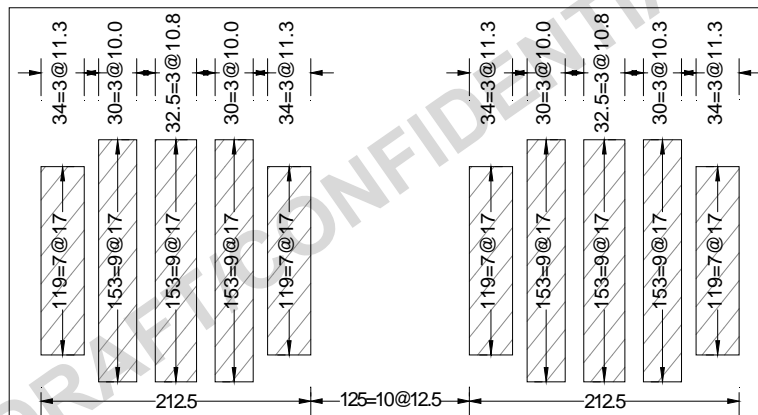


Maximum Vertical Pressure & Footprint Dimensions

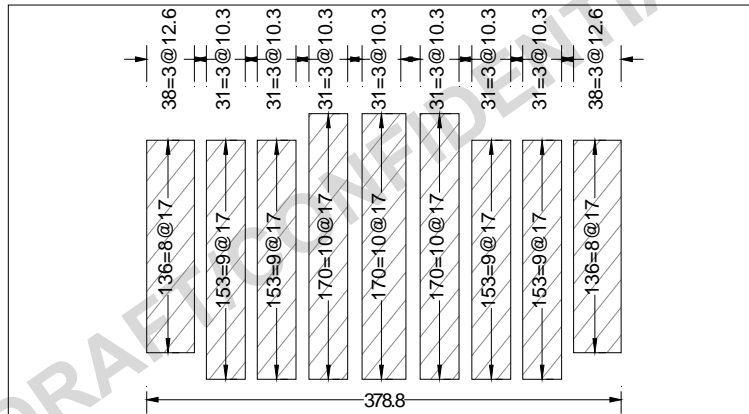
		Rib 1	Groove 1	Rib 2	Groove 2	Rib 3	Groove 3	Rib 4	Groove 4	Rib 5
DTA	Vertical pressure (kPa)	641	11.4	872	14.6	988	14.6	858	11.4	644
	Length (mm)	119		153		153		153		119
	Width (mm)	34		30		32.5		30		34
WBT	Vertical pressure (kPa)	502	9.6	832	9.6	886	10.3	936	11.4	956
	Length (mm)	136		153		153		170		170
	Width (mm)	38		31		31		31		35



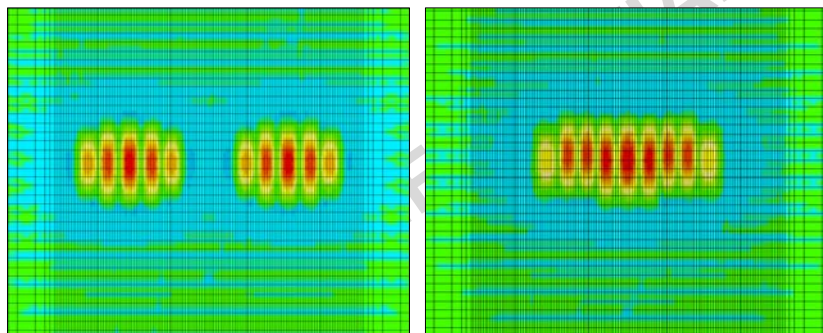
DTA Loading Footprint



WBT Loading Footprint



3D Loading on Thick Pavement Mesh

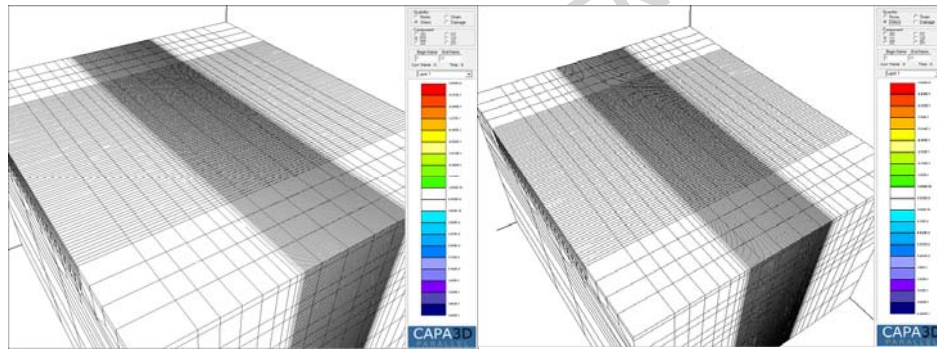


DTA

WBT



Moving DTA and WBT Loading

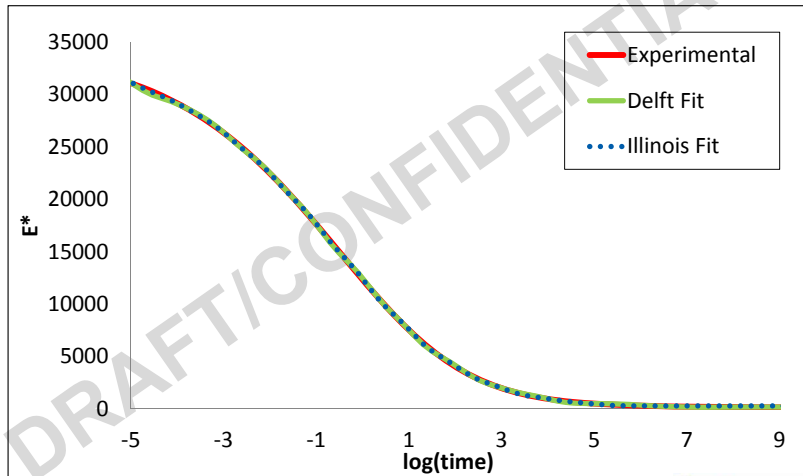


Material Characteristics

Layer	Modulus (MPa)	Poisson's Ratio
Surface Mix (SM-9.5D)	4230.0	0.33
Base Mix (BM-25.0)	4750.0	0.30
Asphalt-Treated Drainage Layer (OGDL)	2415.0	0.30
21A Cement Treated Base Layer (21B)	10342.0	0.20
21B Aggregate Subbase Layer (21B)	310.0	0.35
Subgrade	262.0	0.35



Surface Layer Viscoelastic Characterization

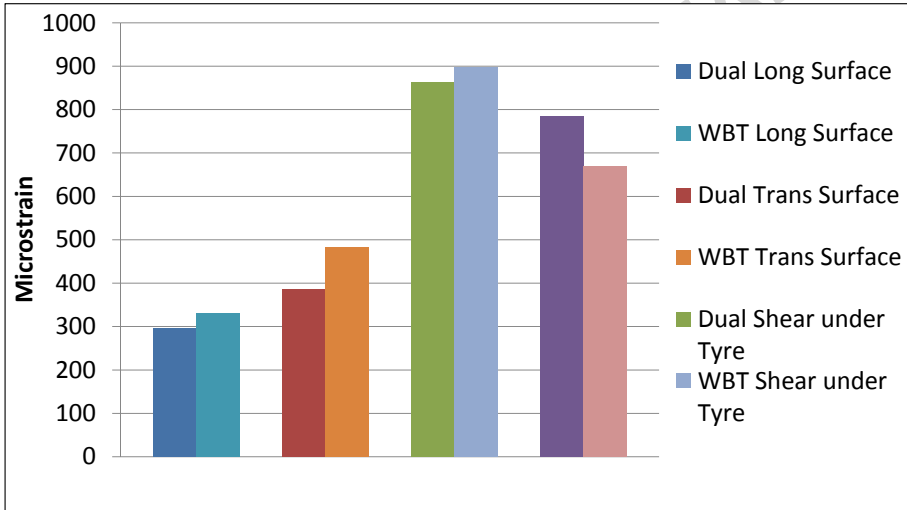


Positions Where Outputs Are Required

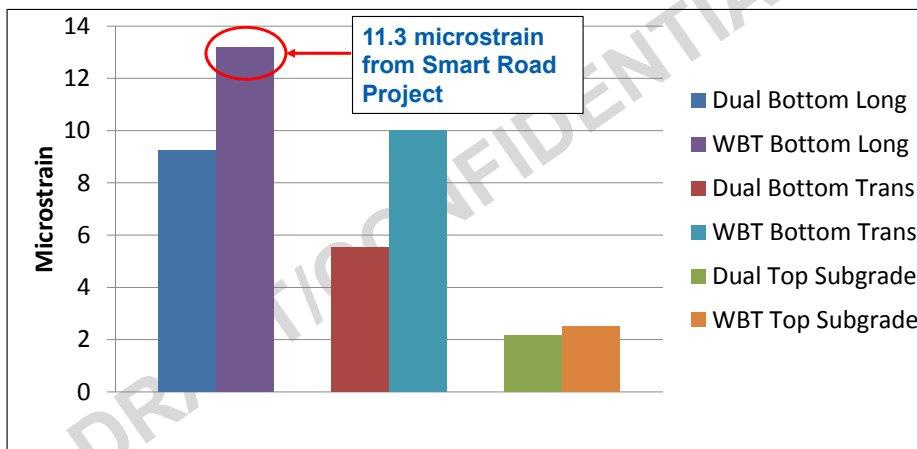
- Maximum tensile strain on transverse and longitudinal directions of **asphalt concrete surface**.
- Maximum tensile strain on transverse and longitudinal directions at of **bottom of the asphalt concrete layers**.
- Maximum vertical compressive strain at **top of subgrade**.
- **Maximum shearing strain in asphalt concrete layers: under the tire and beside the tire**.



Output from Dual and WBT Loadings



Output from Dual and WBT Loadings



Loading Positions for DTA Relative to Center

Strain Label (Dual)	Depth from Surface location	Distance from Loading Center in Traveling Direction	Distance from Center of Loading in Transverse Direction
Long Surface	Surface	-78mm	-0.3mm
Trans Surface	Surface	-10mm	15mm (between rib 3-4)
Shear under tire	34mm	+41mm	0.3mm
Shear beside tire	34mm	+24mm	111mm (5mm from the tire edge)
Bottom Long	Bottom of Asphalt	-37mm	-50mm
Bottom Trans	Bottom of Asphalt	-37mm	-7mm
Top Subgrade	Top of Subgrade	+42mm	173mm (center of DTA)

Note: Minus indicates a position beyond the center



Loading Positions for WBT Relative to Center

Strain Label (WBT)	Depth Location from Surface location	Distance from Loading Center in Traveling Direction	Distance from Center of Loading in Transverse Direction
Long Surface	Surface	-87mm	0.6mm
Trans Surface	Surface	-19mm	29mm (between rib 5-6)
Shear under tire	34mm	-32mm	-0.6mm
Shear beside tire	34mm	-19mm	192mm (2mm from the tire edge)
Bottom Long	Bottom of Asphalt	-45mm	-0.6mm
Bottom Trans	Bottom of Asphalt	-45mm	-0.6mm
Top Subgrade	Top of Subgrade	+34mm	-0.6mm

Note: Minus indicates a position beyond the center



Remarks

- An **efficient** and **accurate** mesh has been developed for **CAPA-3D** per the specifications outlined by TU Delft
- Discretization of the non-uniform contact stress measurements supplied for the DTA and the WBT into a **moving 3D non-uniform contact stress pulse**.
- **Viscoelastic** model parameter determination for the surfacing layer using LTTP 26.0 data provided by UIUC. The CAPA-3D model matched the experimental and the Illinois results
- Determination of mesh locations for output of **maximum strains** at pre-agreed key locations



Future Plans

- TU Delft will continue analysis using the contact stress matrix for DTA and WBT upon complete verification of the model
- TU Delft will proceed to produce the cloud of data needed for the **Artificial Neural Networks** tool



COMMENTS!

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**Pavement Modeling
(UIUC)**

5/30/2013

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Outline

- **Finite element modeling (FEM)**
 - **Dynamic-implicit** analysis
 - **Material** characterization
 - **3D contact stresses**
 - **Continuous** moving loading
 - **Infinite boundary elements**
 - **Layer interaction**
- **Mesh** sensitivity analysis
- **FEM analysis matrix**
 - **Pavement structures**
 - **Load cases**

Outline

- **Python** Development Environment
- **FEM input**
 - **Load**
 - **Materials**
 - **Temperature**
- **Sample results**
- **Response of thin pavements**
- **Response of thick pavements**

Finite Element Modeling



Dynamic-Implicit Analysis

- Considers **mass inertia** and **damping** forces effect on pavement response
- Different contact areas of tire imprint can affect **inertia force** values
- Pavement response is affected by **loading amplitude**



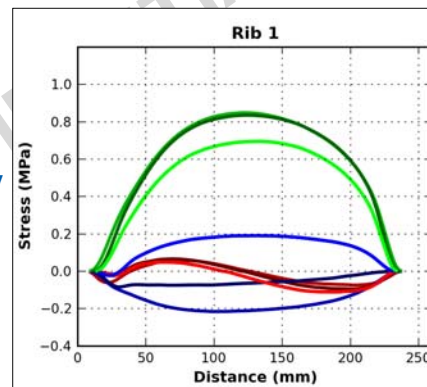
Materials Characterization

- **AC: Linear-Viscoelastic:**
 - E^* test
 - Prony Series Expansion
- **Granular Materials:**
 - **Thin Pavement: Nonlinear stress-dependent**
 - **Thick Pavement: Linear Elastic**

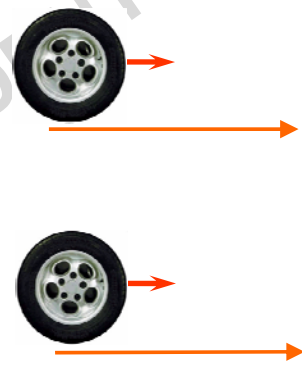
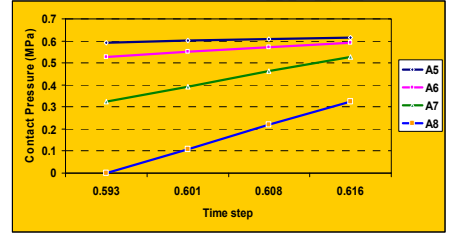
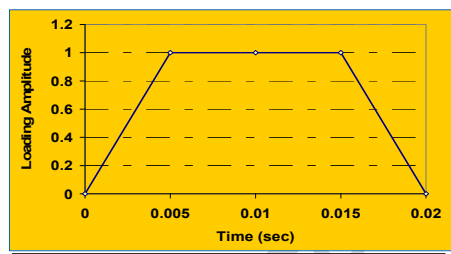


3D Contact Stresses

- **Uniform constant stresses** underestimate response close to the surface
- **3D contact stresses** may create greater compressive strain on top of subgrade and transverse tensile strain

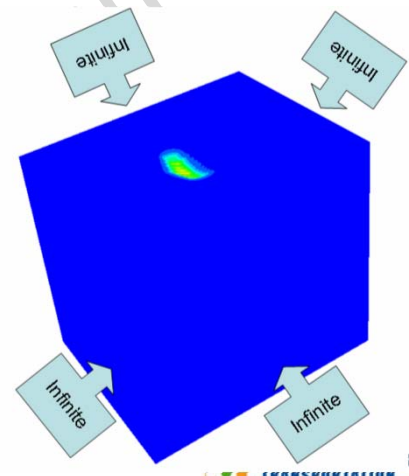


Continuous Moving Loading



Finite Element Model

- **Infinite** Boundary Elements
 - Simulates far-field region
- **Layer Interaction:**
 - Fully-bonded
 - Simple Friction
 - Elastic Slip



Mesh Sensitivity Analysis



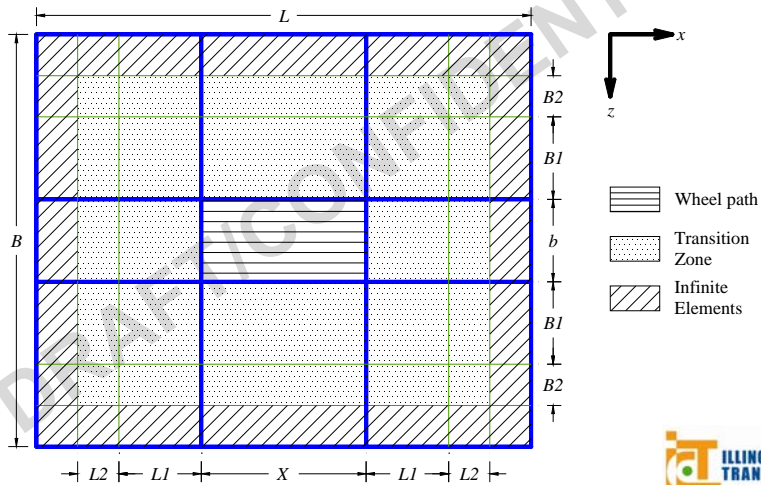
Mesh Sensitivity Analysis

- **Optimum** (computational- and accuracy-wise) distribution and location of finite elements
- Parametric study in **Abaqus** using **BISAR** as reference
- **Responses compared**: tensile strains at bottom of AC; shear strain in each layer; and vertical strain on top of subgrade
- **5% difference** used as criteria for optimum mesh
- Mesh in plan view defined by tire's footprint and transition to model's boundary



Mesh Sensitivity Analysis

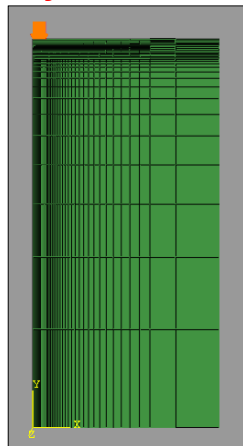
□ Model parameters in plan view



Mesh Sensitivity Analysis

□ Two-step approach

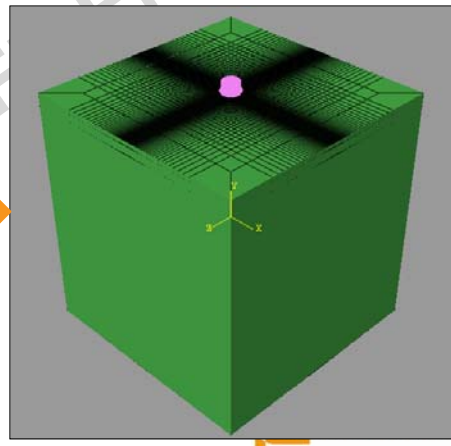
Axisymmetric model



Iterations

Final Check

3D Model



Mesh Sensitivity Analysis

- Abaqus (3D) vs. BISAR: **thin** pavements

	AC=75 mm, Base=150 mm			AC=75 mm, B=600 mm.			AC=125 mm, Base=150 mm			AC=125 mm, Base=600 mm		
	Abaq.	BIS.	Dif.*	Abaq.	BIS.	Dif.*	Abaq.	BIS.	Dif.*	Abaq.	BIS.	Dif.*
$\epsilon_{11,ac}$	126.5	133.8	5.5	105.4	111.3	5.3	63.9	67.2	4.9	56.6	59.5	4.9
$\epsilon_{22,subg}$	817.9	836.8	2.3	354.6	364.4	2.7	341.0	348.9	2.3	206.5	212.6	2.9
$\epsilon_{23,ac}$	27.0	27.4	1.4	25.5	26.1	2.3	17.0	17.0	0.2	16.4	16.5	0.7
$\epsilon_{23,base}$	193.0	190.4	1.4	179.1	170.7	4.9	68.4	67.9	0.8	75.2	73.0	3.0
$\epsilon_{23,subg}$	269.9	276.6	2.4	128.7	135.1	4.8	101.6	103.9	2.2	70.6	75.8	6.9

*Difference in %



Mesh Sensitivity Analysis

- Abaqus (3D) vs. BISAR: **thick** pavements

	AC=125 mm, Base=150 mm			AC=412 mm, Base=600 mm			AC=125 mm, B=150 mm			AC=412 mm, Base=600 mm		
	Abaq.	BIS.	Dif.*	Abaq.	BIS.	Dif.*	Abaq.	BIS.	Dif.*	Abaq.	BIS.	Dif.*
$\epsilon_{11,ac}$	65.6	68.1	3.7	61.1	63.8	4.2	9.9	9.4	5.2	9.1	9.7	6.3
$\epsilon_{22,subg}$	300.0	295.5	1.5	157.4	159.7	1.4	36.0	36.1	0.3	27.9	27.8	0.3
$\epsilon_{23,ac}$	19.4	19.2	1.0	19.8	19.4	1.8	7.3	7.6	4.0	7.6	7.3	4.2
$\epsilon_{23,base}$	73.3	70.0	4.7	74.9	74.7	0.3	6.8	6.6	3.3	7.9	8.0	1.3
$\epsilon_{23,subg}$	83.2	88.2	5.7	53.7	56.6	5.1	8.5	8.1	5.0	7.8	8.2	4.8

*Difference in %



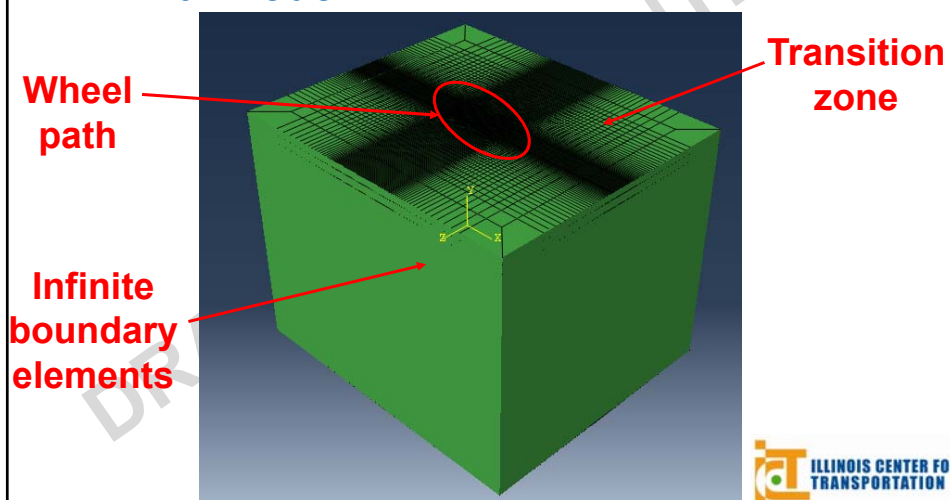
Mesh Sensitivity Analysis


□ Final configuration **thin** pavement:

Thin Pavements		Model			
		AC=75 mm, Base=150 mm	AC=75 mm, Base=600 mm	AC=125 mm, Base=150 mm	AC=125 mm, Base=600 mm
Dimensions (mm)	<i>L</i>	4300	5800	4800	5300
	<i>B</i>	4300	5800	4800	5300
	<i>D</i>	4500	4500	4500	4500
	<i>L1 = B1</i>	1200	1950	1450	1700
	<i>L2 = B2</i>	300	300	300	300
AC	No. Elem.	12	12	15	15
	Bias	1.0	1.0	1.2	1.2
Base	No. Elem.	12	25	12	25
	Bias	1.7	1.3	1.7	1.0
Subgrade	No. Elem.	15	15	15	15
	Bias	70.0	30.0	50.0	30.0
<i>L1 = B1</i>	No. Elem.	25	30	30	25
	Bias	10.0	20.0	10.0	15.0
<i>L2 = B2</i>	No. Elem.	1	1	1	1
	Bias	1.0	1.0	1.0	1.0


Mesh Sensitivity Analysis


□ Final Model





FEM Analysis Matrix

 ILLINOIS CENTER FOR
TRANSPORTATION




FEM Analysis Matrix

- Structures considered: **Thin** pavement

Thin Pavement Structure		
	Different Materials	Thicknesses
AC Layer	W, S*	75 and 125 mm
Base	W, S*	150 and 600 mm
Subgrade	35 and 140 MPa	--
Possible combination	32	
With load cases (12)	384	

*W = Weak; S = Strong

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FEM Analysis Matrix

- Structures considered: **Thick** pavement

Thick Pavement Structure		
	Different Materials	Thicknesses
Wearing Surface	W1, S1*	25 and 62.5 mm
Intermediate Layer	W2, S2*	37.5 and 100 mm
Binder Layer	W3, S3*	62.5 and 250 mm
Base and Subbase	140 and 415 MPa	150 and 600 mm
Subgrade	70 MPa	--
Possible Combination		16
With Load cases (12)		192

*W = Weak; S = Strong



FEM Analysis Matrix

- Loading Cases

Load Case	Tire Type	Applied Load (kN)	Tire Inflation Pressure (kPa)
L1	WBT	26.6	552
L2	WBT	26.6	862
L3	WBT	79.9	552
L4	WBT	79.9	862
L5	DTA	26.6	552
L6	DTA	26.6	862
L7	DTA	26.6	562/758
L8	DTA	79.9	562
L9	DTA	79.9	862
L10	DTA	79.9	562/758
L11	WBT	44.4	758
L12	DTA	44.4	758



Pavement Modeling (Thin & Thick)

10:15-11:00am

5/30/2013



Abaqus Python Development Environment (PDE)



Abaqus PDE

- **Abaqus PDE***
 - **Automate** repetitive tasks
 - Perform parametric studies
 - Create and modify models
 - Access **data** in an **output database**

*Abaqus 6.11 Documentation



Generation of Input Files (Abaqus PDE)

- **Geometry and materials:** Model dimensions, layer thicknesses, material definition, and layer interaction
- **Mesh:** element type and size in each layer, mesh configuration in tire's footprint, and transition to model boundary
- **Load:** 3D contact stresses in footprint, continuous moving load, temperature



Abaqus PDE

- Extract information from output database (post-processing):
 - Extreme **responses** in each layer
 - **Locations** of responses
 - **Variation** of responses **along paths** (e.g. depth)

FEM Input

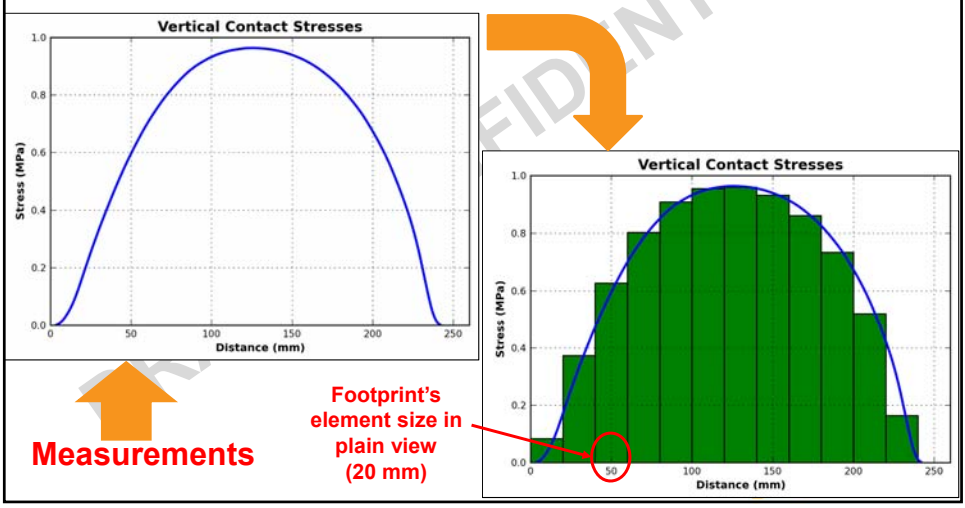
FEM Input

- **Load:** Contact stress measurements
- **AC materials:** **LTPP** Database
- **Granular materials:** **Nonlinear** cross-anisotropic laboratory characterization
- **Temperature** profile: Analytical temperature distribution model



FEM Input

- **Load**

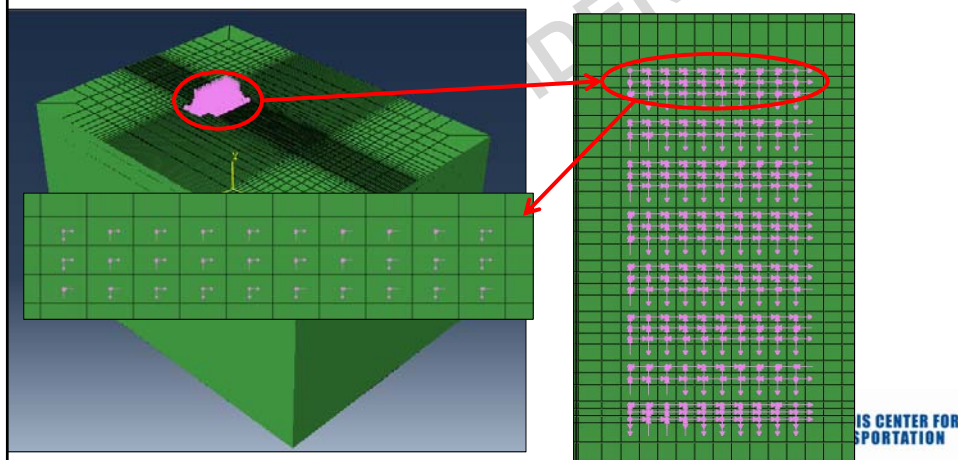


FEM Input

□ From measurements to FEM

Finite Element Model

Contact Stresses



FEM Input

□ AC Materials

□ Long-Term Pavement Performance (LTPP)

Data Release #26

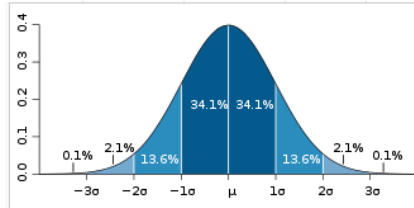
- Two sets representing the **extreme limits** → (a) weak and (b) strong

□ Methodology

- **Statistical Analysis**
- **NMAS** Criterion (typical values per layer)

FEM Input

- Based on more than **1000 data sets**



$2\sigma \approx 95.4\%$,
 $2.5\sigma \approx 97.5\%$
and $3\sigma \approx 99.8\%$

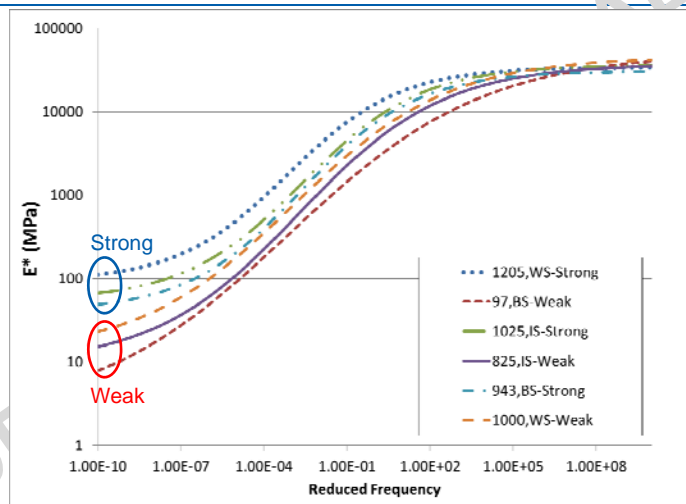
- Layer Properties: **NMAS**

- Wearing Surface (WS) 9.5 or 12.5mm
- Intermediate Layer (IS) 25 or 19.5mm
- Base Layer (BS) 25 or 37.5mm

From http://en.wikipedia.org/wiki/Normal_distribution.



FEM Input: AC Materials



FEM Input

- Base materials (**thin pavements**)
 - **Cross-anisotropic stress-dependent**

$$M_r = k_1 p_a \left(\frac{\theta}{p_a} \right)^{k_2} \left(\frac{\tau_{oct}}{p_a} + 1 \right)^{k_3}$$

- Based on database of **114 materials** (Tutumluer, 2008)
- Materials in database tested using **pulse load in vertical and radial directions**



FEM Input

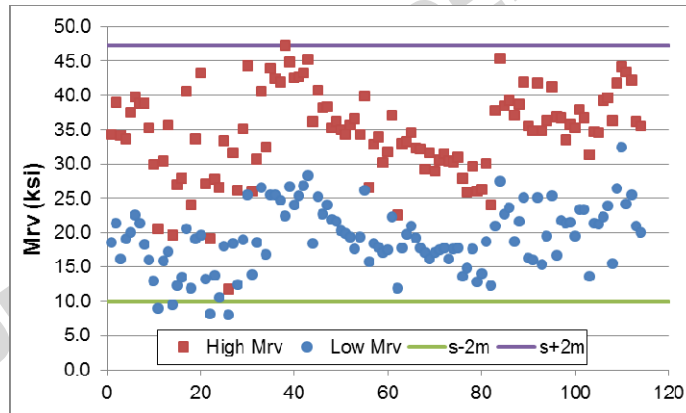
- Two stress levels defined to select weak and strong material (Xiao et al., 2011)

	Low stress level	High stress level
	kPa	kPa
σ_3	34.9	104.8
σ_d	104.8	209.5
σ_1	139.7	314.3
σ_2	34.9	104.8
θ	209.5	523.9



FEM Input

- Vertical resilient modulus of each material at **both stress levels**



FEM Input

- Vertical and horizontal shear modulus from **laboratory tests**
- Shear resilient modulus from **simplified procedure** (Tutumluuer and Thompson, 1998)

Direction	Weak			Strong		
	k_1	k_2	k_3	k_4	k_5	k_6
Vertical	453.3	0.8858	-0.5713	869.6	0.9785	-0.5673
Horizontal	282.4	0.6701	-1.1341	596.6	1.1419	-1.3464
Shear	310.3	1.0297	-1.1036	389.1	0.9083	-0.2409

FEM Input

- **Temperature** distribution in AC (Wang, 2013)
 - **Two layer system:** AC layers and granular
 - Bound temperature distribution
 - Initial temperature distribution function of depth z only
 - Continuous heat flow at the interface between layers



Temperature Distribution

- **Governing Equations**
 - Temperature distribution in each layer:

$$\frac{\partial T_1}{\partial t}(z, t) = \alpha_1 \frac{\partial^2 T_1}{\partial z^2}(z, t) \quad 0 < z < H$$

$$\frac{\partial T_2}{\partial t}(z, t) = \alpha_2 \frac{\partial^2 T_2}{\partial z^2}(z, t) \quad z > H$$
 - Initial temperature in each layer:

$$T_1(z, 0) = G_1(z) \quad 0 < z < H$$

$$T_2(z, 0) = G_2(z) \quad z > H$$



Temperature Distribution

- **Continuous temperature** and heat flow at interface:

$$T_1(H, t) = T_2(H, t)$$

$$\lambda_1 \frac{\partial T_1}{\partial z}(H, t) = \lambda_2 \frac{\partial T_2}{\partial z}(H, t)$$

- **Energy Balance at pavement surface:**

$$\lambda_1 \frac{\partial T_1}{\partial z}(0, t) = B[T(t) - T_1(0, t)]$$

Temperature Distribution

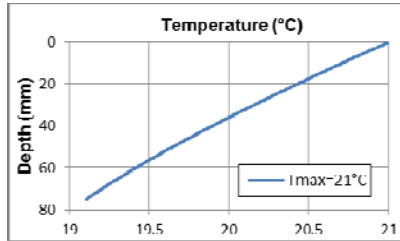
- **Solution for AC layer:**

$$\hat{U}_1(z, s) = \frac{B\hat{f}(s) \left[e^{\sqrt{\frac{s}{\alpha_1}}z} - L e^{(2H-z)\sqrt{\frac{s}{\alpha_1}}} \right]}{B - \lambda_1 \sqrt{\frac{s}{\alpha_1}} - e^{2H\sqrt{\frac{s}{\alpha_1}}} L \left(B + \lambda_1 \sqrt{\frac{s}{\alpha_1}} \right)}$$

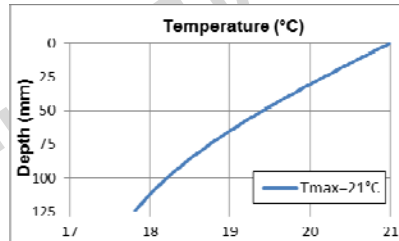
$$\text{with } L = \frac{1 + \frac{\lambda_1 r_1}{\lambda_2 r_2}}{1 - \frac{\lambda_1 r_1}{\lambda_2 r_2}}$$

Temperature Distribution

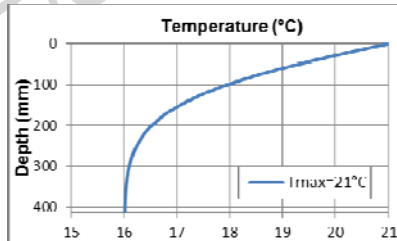
H=75 mm



H=125 mm



H=412 mm



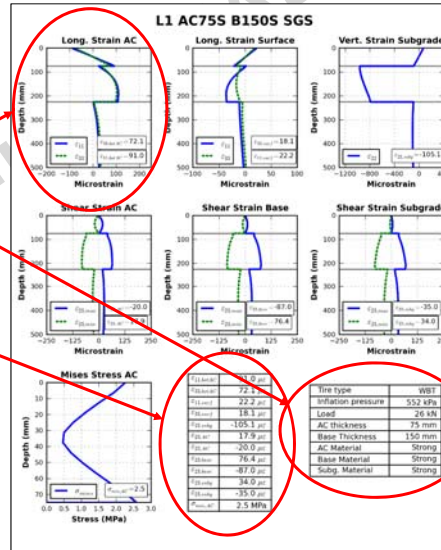
Sample of Results



Sample of Results

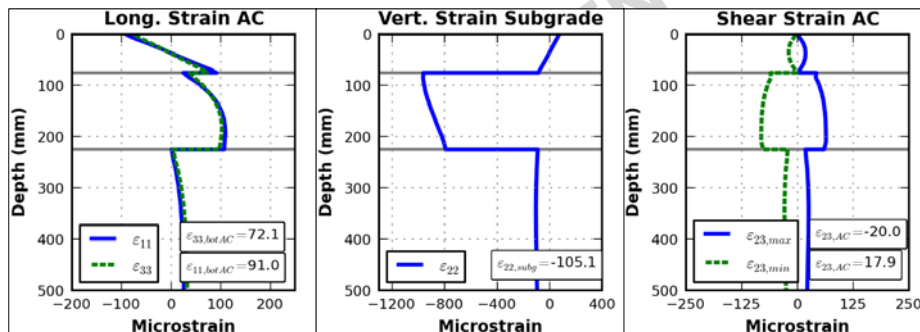
For each one of the **576 cases**

Tire Inflat	$\epsilon_{11,botAC}$	91.0 $\mu\epsilon$	WBT
Load	$\epsilon_{33,botAC}$	72.1 $\mu\epsilon$	552 kPa
AC thickness	$\epsilon_{11,surf}$	22.2 $\mu\epsilon$	26 kN
Base Material	$\epsilon_{33,surf}$	18.1 $\mu\epsilon$	75 mm
Subgrade Material	$\epsilon_{22,subg}$	-105.1 $\mu\epsilon$	150 mm
Subgrade Strength	$\epsilon_{23,AC}$	17.9 $\mu\epsilon$	Strong
Subgrade Stiffness	$\epsilon_{23,AC}$	-20.0 $\mu\epsilon$	Strong
Subgrade Stiffness	$\epsilon_{23,base}$	76.4 $\mu\epsilon$	Strong
Subgrade Stiffness	$\epsilon_{23,base}$	-87.0 $\mu\epsilon$	Strong
Subgrade Stiffness	$\epsilon_{23,subg}$	34.0 $\mu\epsilon$	Strong
Subgrade Stiffness	$\epsilon_{23,subg}$	-35.0 $\mu\epsilon$	Strong
Subgrade Stiffness	$\sigma_{mis,AC}$	2.5 MPa	00



Sample of Results

L1 AC75S B150S SGS



Responses of Thin Pavements

Responses of Thin Pavements

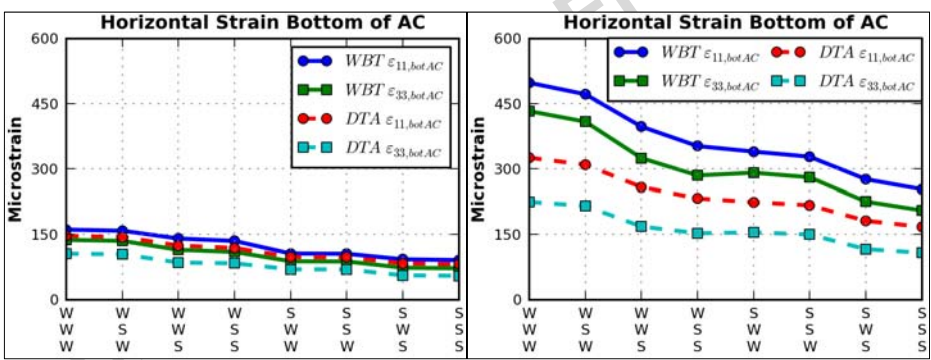
- **Thinnest** pavement (AC=75 mm and Base=150 mm) **all material combinations:**
 - WBT vs. DTA at **low** load and tire-inflation pressure (P=26.6 kN, $\sigma=552$ kPa)
 - WBT vs. DTA at **high** load and tire-inflation pressure (P=79.9 kN, $\sigma=862$ kPa)
- **All load combinations** for the same pavement structure

Strain at the bottom of AC

AC75 B150

P=26.6 kN, $\sigma=552$ kPa

P=79.9 kN, $\sigma=862$ kPa

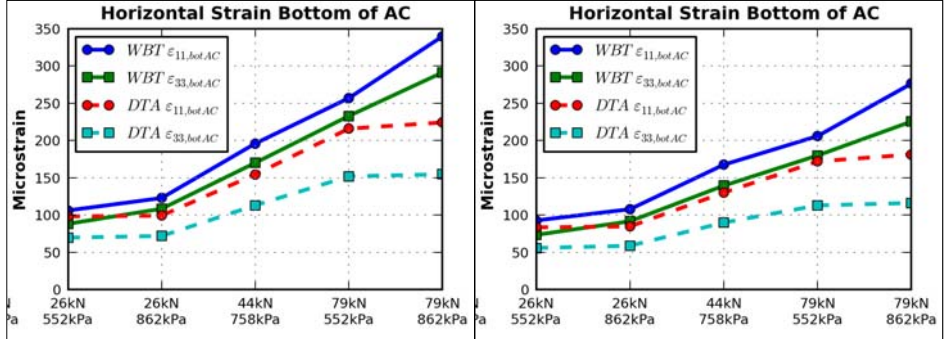


Effect of Loading Cases

- Tensile strain at bottom of AC

AC75S B150W SGW

AC75S B150W SGS



Weak Subgrade

Strong Subgrade



Responses of Thick Pavement

Responses of Thick Pavements

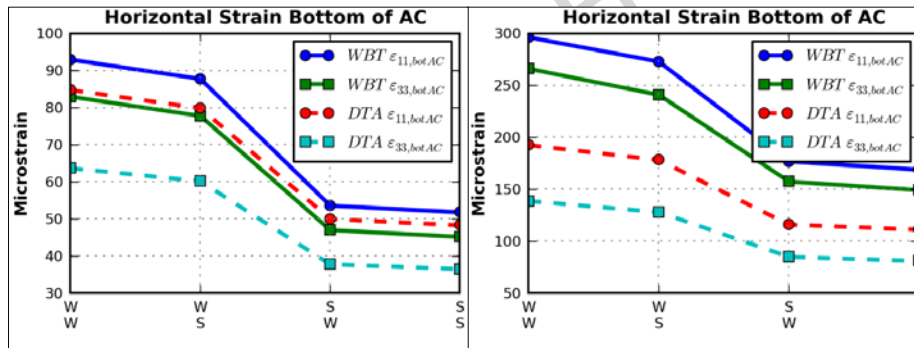
- **Thinnest** pavement (AC=125 mm and Base=150 mm) **all material combinations:**
 - WBT vs. DTA at **low** load and tire-inflation pressure (P=26.6 kN, σ =552 kPa)
 - WBT vs. DTA at **high** load and tire-inflation pressure (P=79.9 kN, σ =862 kPa)
- **All load combinations** for the same pavement structure (AC=412 mm and Base=150 mm)

Effect of Material Properties

AC125 B150

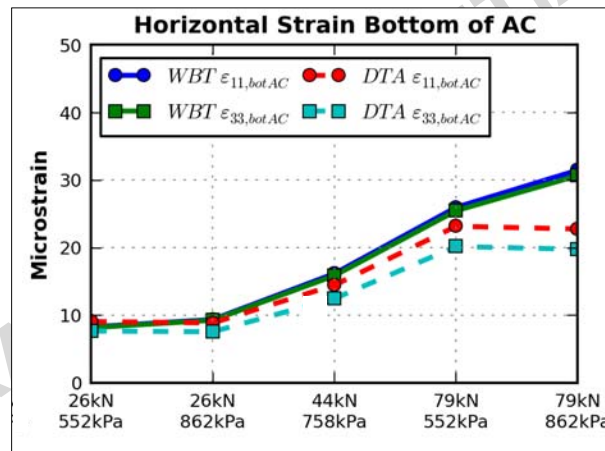
P=26 kN, $\sigma=552$ kPa

P=79 kN, $\sigma=862$ kPa



Effect of Loading Cases

AC412S B150W



Remarks

- **Small difference** between **horizontal** strains in the longitudinal and lateral directions (top and bottom of AC)
- **Difference** between WBT and DTA become more pronounced with **higher load** and **higher tire** pressure

Future Plans

- Complete **thin and thick pavement cases** with various combinations of **axle loads** and **tire inflation pressures**
- Provide **comprehensive analysis** with regards to the effect of:
 - Tire type
 - Material property
 - Loading case
 - Pavement structure

COMMENTS!


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Data Management
11:00-12:00am

5/30/2013

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Outline

- Introduction and Objectives
- Existing data
- New data
- Filtering process
- Interface design
- Future Plans: Artificial Neural Network

The Need for Field and APT Data

- Represent **real conditions**
- Realistic **responses** from field
- Model validation
- Utilize as **training** or for the **testing** phase of Artificial Neural Networks

Objectives of Data Management

- Data **filtering** as needed and process **automation**
- Data management and organization
- Allow easy access to data by designing an **interface**
- Provide a platform for future data **updates**

Data Sources

- Five main data sources:
 - UIUC-Thin Pavement Sections
 - Florida DOT
 - UC-Davis
 - Ohio SPS-8
 - Virginia Tech - Smart Road
- Huge amount of data/information
- **Update** w/ new data as it becomes available

UIUC-Thin Pavement Sections

- **Nine** low-volume AC sections
- Three tire types: **Dual**, **WBT-425**, and **WBT-455**
- Various loads, speeds, and tire inflation pressures
- Instrumentation: **Strain gauges**, **LVDT**, **pressure cells**, and **thermocouples**



UIUC-Thin Pavement Sections-Data

- **Strain** at the bottom of surface layer
- Vertical **deflection** on top of subgrade
- Longitudinal and transverse base **deformations**
- Surface **rutting**



Florida DOT

- **Six** test lanes
- **Open-** and **dense-graded AC** layers
- **Tires: Dual, WBT-445, WBT-455**
- **Instrumentation: Surface strain gauges** (longitudinal and transverse)
- **Rutting** data

UC-Davis

- **Rutting of two overlay systems: dense-graded AC (DGAC) and asphalt-rubber hot mix gap-graded (ARHM-GG)**
- **Tire types: Dual radial, dual bias-ply, WBT-425, and aircraft tires**
- **Profile data**
- **3D contact stresses**

Ohio SPS-8

- Two sections of **4- and 8-in-thick AC** on the **U.S. Route 23** Test Road
- Single-unit **two axle truck** with two tires: **Two dual and two wide-base** (WBT425, WBT495)
- Strain gage **rosettes** in different directions at AC layer
- Tire pressure patterns
- FWD



Virginia Tech Smart Road

- 1999-2002 database
- **Instrumentation**: Strain gauges (AC, base, sub-base); Pressure cells (two types); Time-domain reflectometry (TDR), thermocouples, ...
- **Dynamic data** response
- **Static** environmental data response
- GPR, friction, roughness, and FWD



New Data Sources

- Florida DOT
- UC-Davis
- Ohio

Florida DOT

- **Test Pit and Test Track data**
- Dual and NGWB tires
- Instrumentation: **Embedded and surface** strain gauges
- Pressure cells (bottom of AC and base)

Florida DOT – Test Matrix

Tire Type	Inflation Pressure (kPa)	Tire Loading (kN)				
NGWB and Dual	552	26.6	35.5	44.4	62.2	79.9
NGWB and Dual	690					
NGWB and Dual	758					
NGWB and Dual	862					
Dual Only	414/758*					
Dual Only	552/758*					

*Differential Tire Inflation Pressure

UC-Davis

- 5-in high RAP surface layer and 2-in AC wearing surface layer
- Strain gauges in both directions under the AC layer lifts
- Instrumentation: Longitudinal and transverse strain gauges (bottom of AC and RAP base layers)
- Pressure cells at bottom of aggregate base layer
- Multi-Depth Deflectometer (MDD)

Ohio

- Total of **three sections** (mainline and ramp)
- Test matrix includes:
 - Two tire type (dual and wide)
 - Two axles (single and tandem)
 - Various loads, speeds and tire inflation pressures
- Instrumentation: Two types of **strain gauges**, **Rosettes**, two types **pressure cells**, and **LVDTs**
- Collected data to date: 3 sections out of 4 at **highest load case** (6 out of 48 cases - **10%** completed)



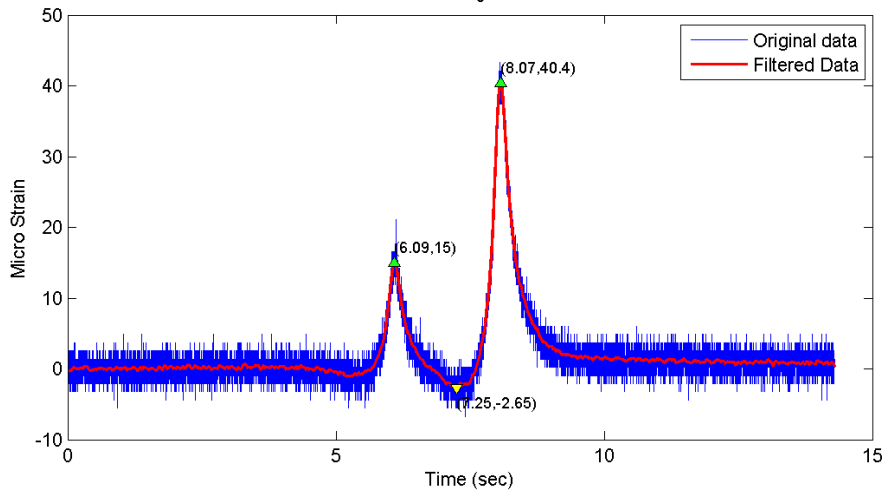
Data Filtering Process

- **Florida** and **Ohio** data filtering is in progress
- Three-step filtering process:
 - **Transferring** data to origin
 - **Smoothing/filtering** using Robust Local Regression Method
 - Extracting **local extrema**
- All processes are done in **Matlab**



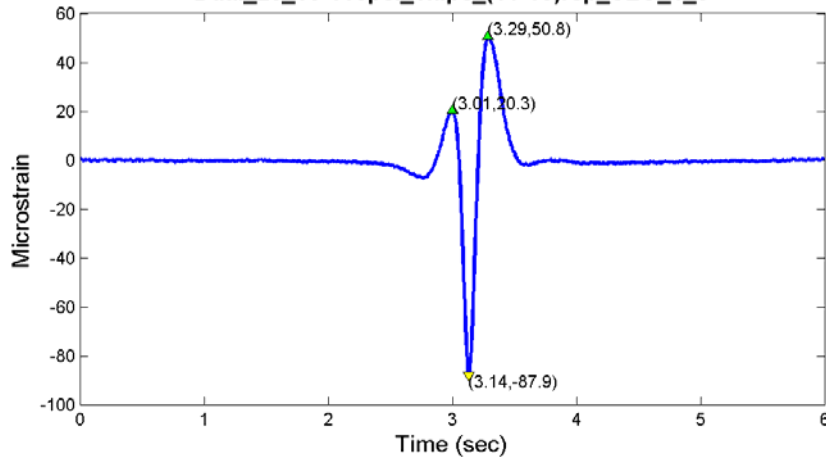
Typical Strain Data - Ohio

SW-14kips-80psi₀5mph-PM-001



Typical Strain Data - Florida

Dual_25_60-110psi_6kips_(11-15)rep_SLG_1_3



Interface Design

- Data organization for easy access
- AutoPlay Media Studio 8 software

Run Demo

Future Plans: Artificial Neural Network

- All useful collected **data** will be utilized
- To **predict pavement damage** caused by various **loading** and **tire configurations**
- Robust, nonlinear, and strong modeling technique
- **Accurate** if trained properly
- **Easier to use** compared to FEM
- Less computational time

Artificial Neural Networks Input

- Pavement **structure** characteristics: number of layers, thicknesses, binder, elastic modulus, agg. properties, etc.
- **Loading, tire** configuration, and **speed**
- Data include: **FEM, field,** and **APT** data
 - **FEM** modeling data will be used for **training**
 - **Field** and **APT** data for **validation** purposes



Artificial Neural Networks Output

- **Responses** related to **fatigue, rutting** and **thermal cracking**;
 - **Transverse strain** at bottom of AC
 - **Vertical strain** (deformation) on top of subgrade
- **Damage Ratio**



COMMENTS!

**ILLINOIS CENTER FOR
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Laboratory Testing
1:00-1:45pm

5/30/2013

**ILLINOIS CENTER FOR
TRANSPORTATION**

Laboratory Testing

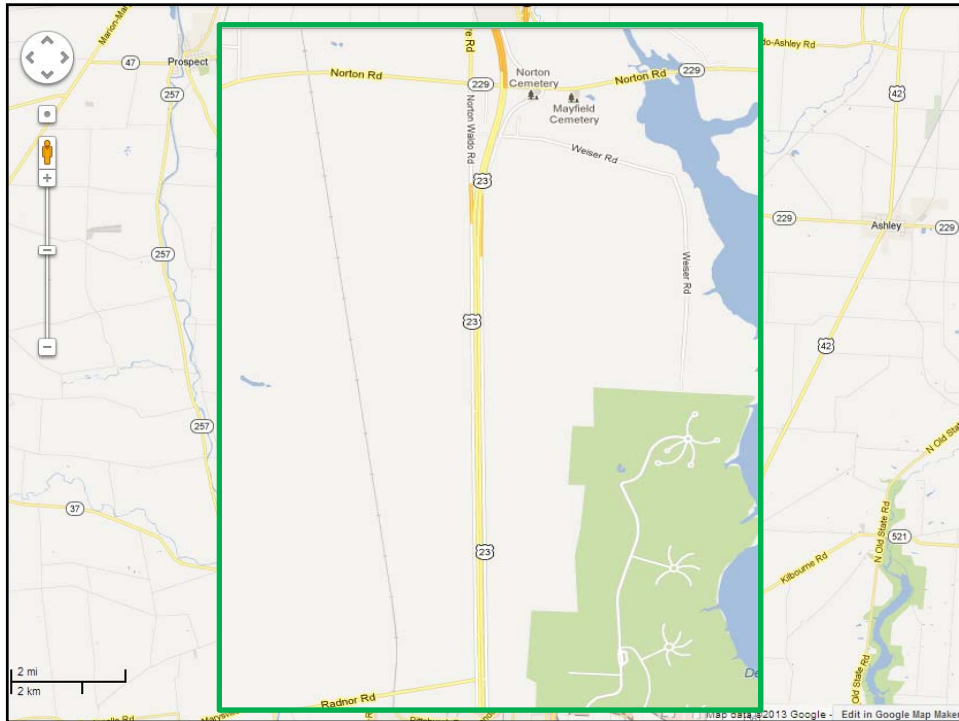
- Sampling Overview
 - Sampling
 - Splitting
 - Compacting
 - Loose Mix, MRL, etc
 - Tracking of trucks
- Cutting & Coring
- Testing



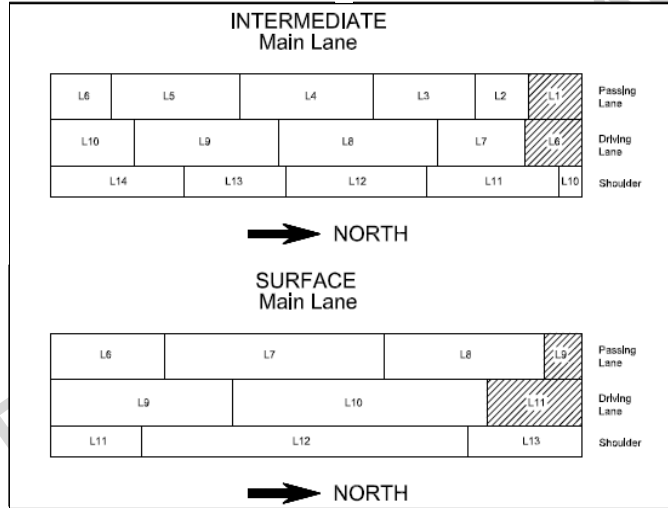
“Mobilized” Lab





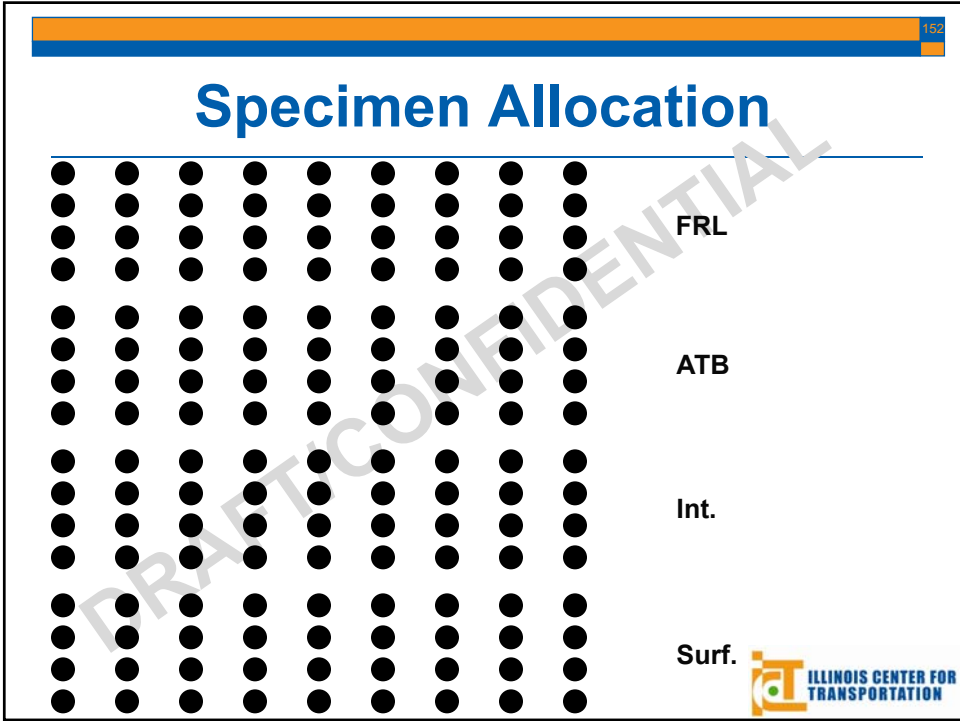
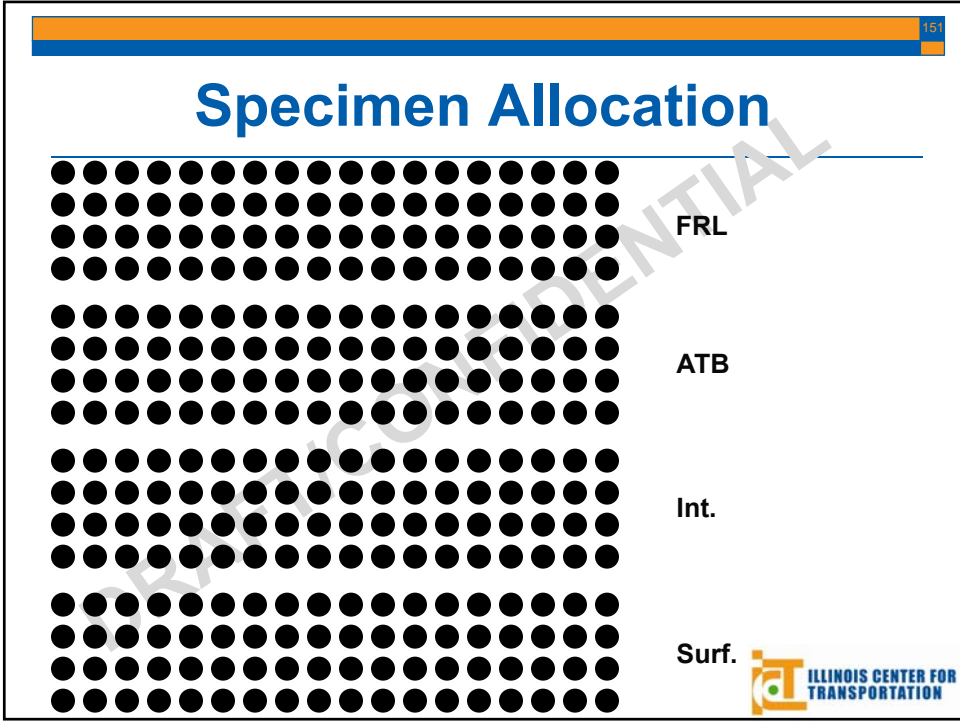


Paving Sequence

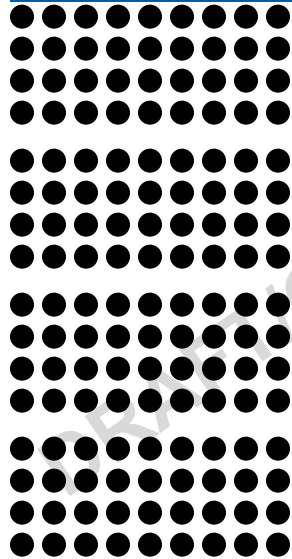


Target Density





Specimen Allocation



Per
Material

FRL

ATB

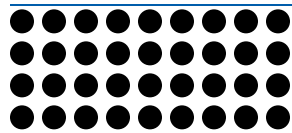
Int.

Surf.



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Specimen Allocation

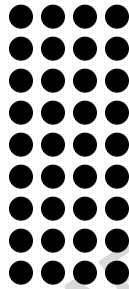


Per
Material

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Specimen Allocation



E*

SCB

IDT

DCT

Push-Pull

Spares-TBD



E* Fabrication



150mm→100mm

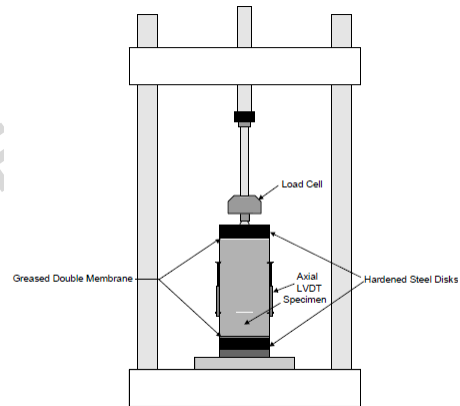


Top/Bottom cuts

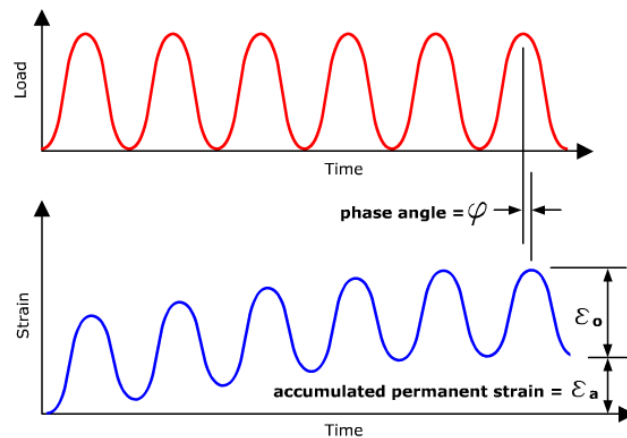


E* Specification

- **AASHTO T 342-11**
(formerly TP 62-07)
 - **NMAS ≤ 37.5 mm**
 - Dense- or gap-graded
 - **Conditions:**
 - **5 temperatures**
 - -10, 4.4, 21, 38, 54 °C
 - (14, 40, 70, 100, 130 °F)
 - **6 frequencies**
 - 25, 10, 5, 1, 0.5, 0.1 Hz
 - **Stress-controlled test**
 - **Haversine axial compressive load**



E* Testing



E* Testing Images



IDT Fabrication

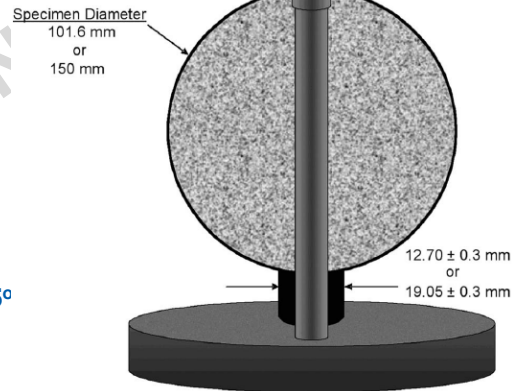


50mm Slice



IDT Specification

- **ASTM D 6931-12**
 - Tensile strength
 - Constant vertical deformation
 - $25 \pm 1^\circ\text{C}$
- **AASHTO T 322-07**
 - Tensile creep
 - Static Load
 - Limited by strain
 - -20, -10, and $0 \pm 0.5^\circ$
 - 3 ± 1 hrs



IDT Testing Images



SCB Fabrication



25-50mm Slice



Notch



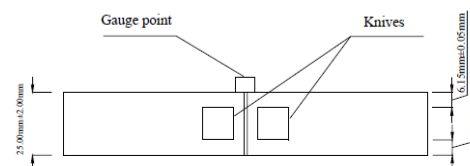
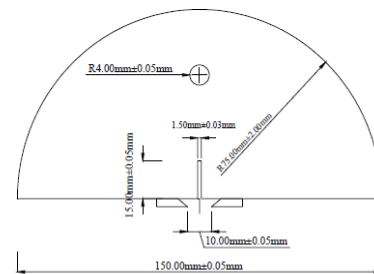
Top/Bottom cuts



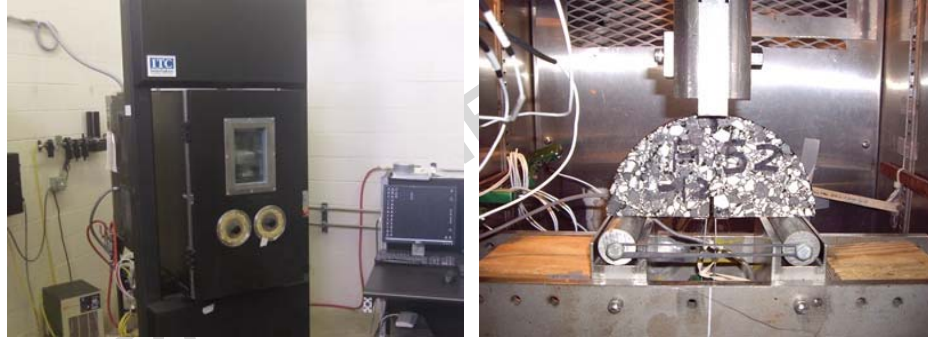
SCB Specification

□ AASHTO Draft

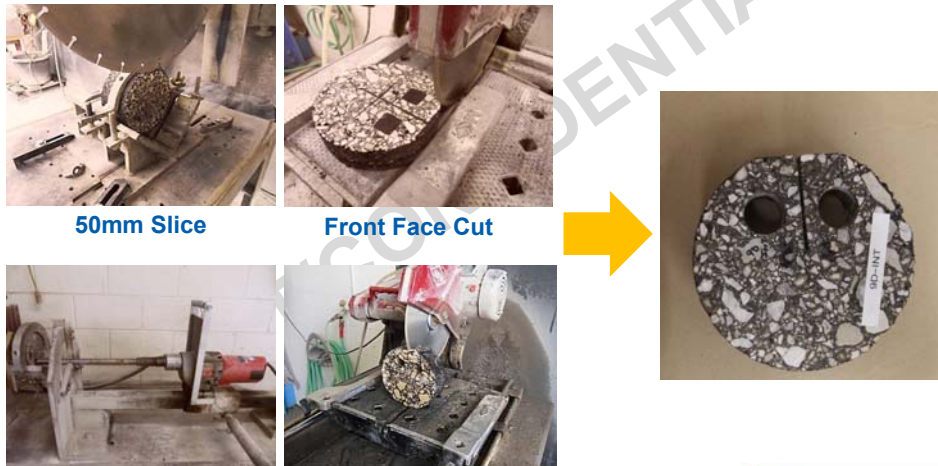
- Displacement control
 - CMOD
 - 0.0005 mm/s
 - 0.03 mm/min
 - Low PG + 10°C
 - Conditioning time = 2 ± 0.2 hrs
 - Temp. = $\pm 1^\circ\text{C}$



SCB Testing Images



DC(T) Fabrication



50mm Slice

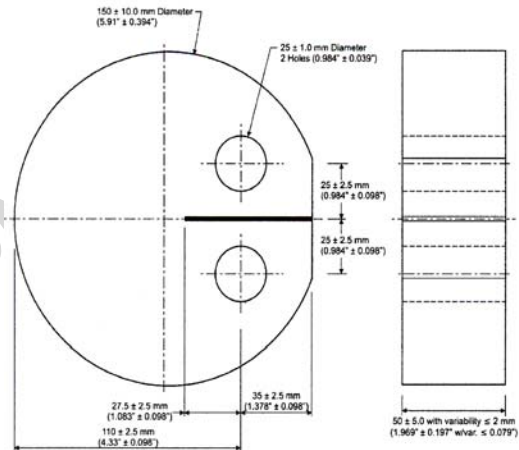
Front Face Cut

Core Drilled Holes

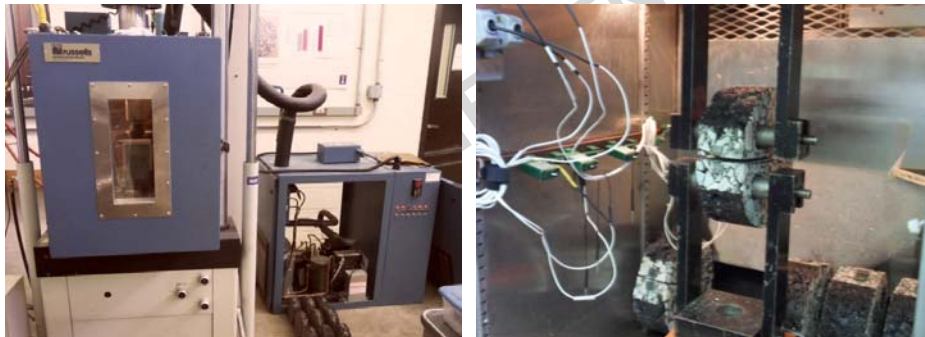
Notch

DC(T) Specification

- **ASTM D 7313**
 - **Test developed in 2005**
 - **Advantages**
 - Provides larger ligament length than SCB
 - Easier geometry than SEB to fabricate from field cores
 - **Displacement controlled test**
 - 1.0mm/min
 - **Required equipment**
 - Load cell with capable resolution
 - Crack mouth opening displacement (CMOD) gauge
 - **Low PG + 10°C**



DC(T) Testing Images



Push-Pull Fabrication



150mm → 100mm



Top/Bottom cuts

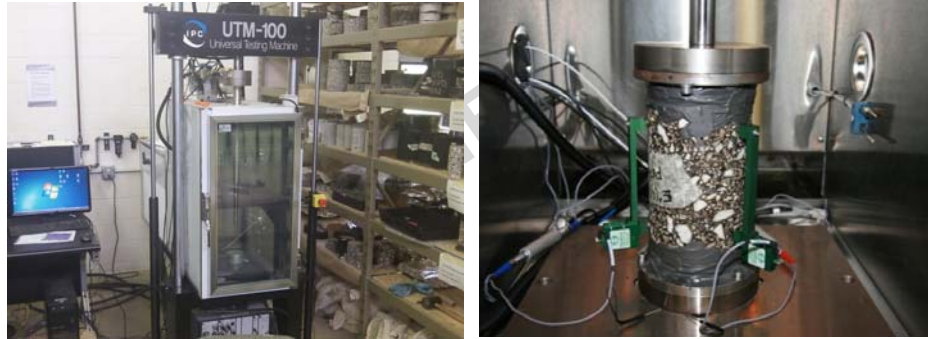


Push-Pull Specification

- **Draft**
 - **Fatigue test**
 - **Continuum damage characteristics**
 - **Simple Uniaxial test**
 - **15 & 20 ± 0.5°C**



Push-Pull Testing Images



Equilibration Time

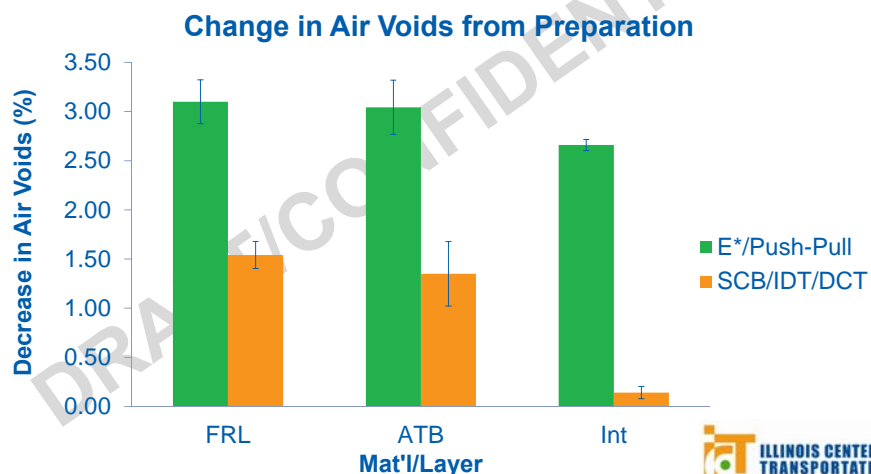


This is Characterization...

- Constant target **density**, regardless of field data
- Allows for cataloging to a **vast database** with other materials that have undergone general characterization
- Monitors **consistency** of production truck-by-truck

Density Results

- Useful to carry into validation phase



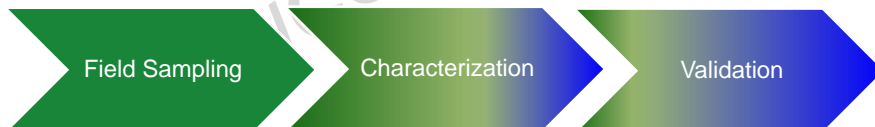
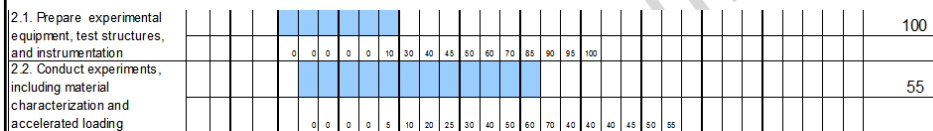
Validation

- ❑ Loose mix collected during production will be compacted to match the nuclear density data from the field at time of placement (no longer $7.0 \pm 0.5\%$)
- ❑ Allows for direct comparison, validation of models

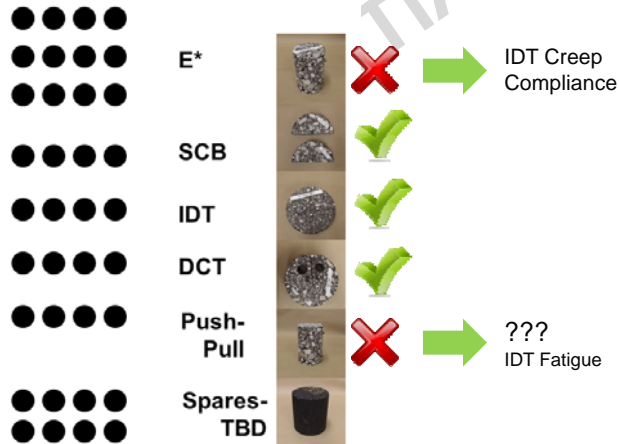
(%AV: FRL=4.5, ATB=4.6, INT=4.5, SURF=4.7)



Laboratory Testing Progress



Adjustments for Field Cores



***Note: Both FL & UC-Davis will be performing E* testing on SGC specimens



Future Plans

- Compact **SGC** specimens that **simulate** the **field**-compacted samples (air void validation)
- Finish **laboratory test matrix** for materials in all testing sites



COMMENTS!



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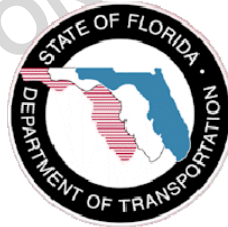
**Instrumentation and Testing:
Ohio, Florida, and Davis**
1:45-3:15pm

5/30/2013



ILLINOIS CENTER FOR
TRANSPORTATION

Instrumentation and Testing: Florida



Topics

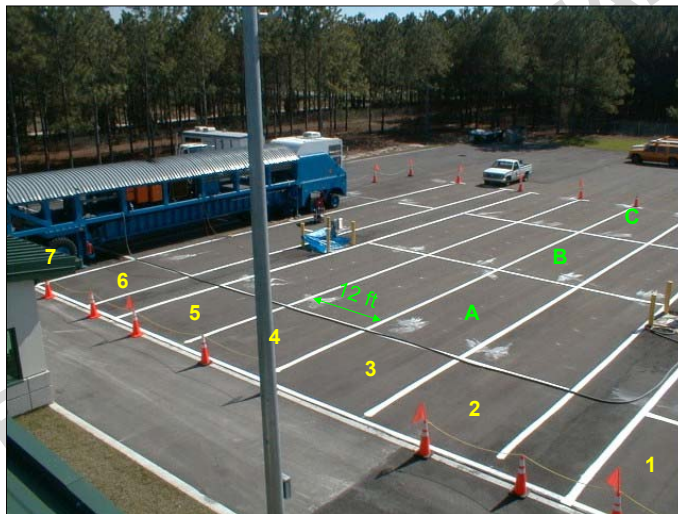
- ❑ FDOT's APT Facility
- ❑ Test Section Design
- ❑ Instrumentation
- ❑ Construction
- ❑ Material Sampling
- ❑ HVS Testing



FDOT's APT Facility

- State Materials Research Park,
Gainesville
- Test sections
 - Eight test tracks
 - Two test pits
- Heavy Vehicle Simulator (HVS)

Test Tracks



Test Pits



Test Track Aerial View



Heavy Vehicle Simulator

- Heavy Vehicle Simulator, Mark IV
 - Wheel speed: 7 mph
 - Loading: 7 to 45 kips
 - Dual or single tires



Dual Tire



Wide-Base Tire



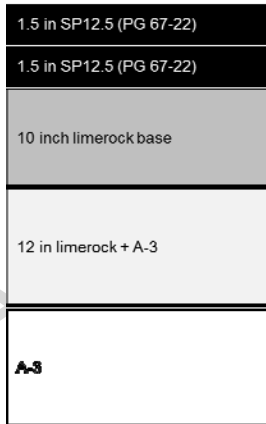
Heating System

- Six 9 ft. long elements attached to HVS test beam
- Independently controlled to provide six heating zones
- Thermocouples monitor asphalt temperature to a depth of 2 in
- Styrofoam filled panels insulate the test area

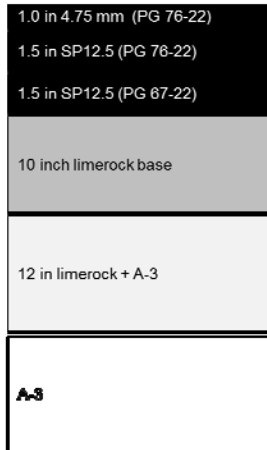


Test Section Design

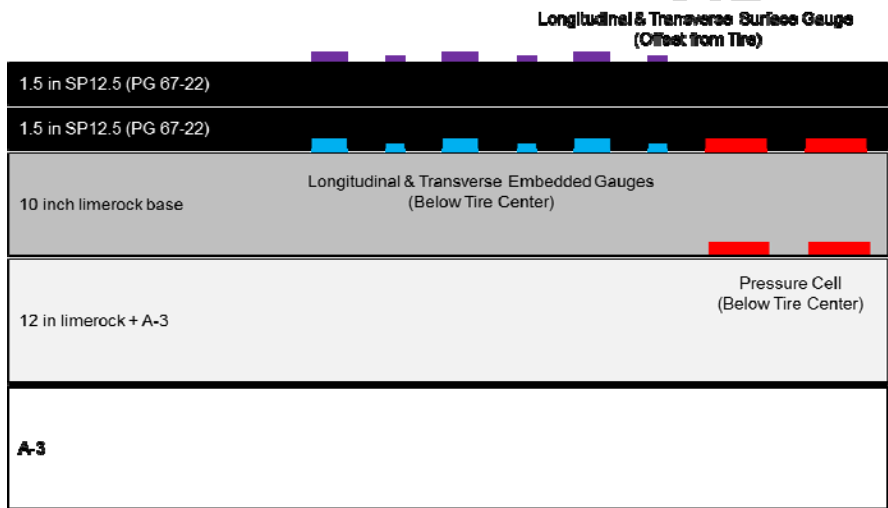
Test Pit



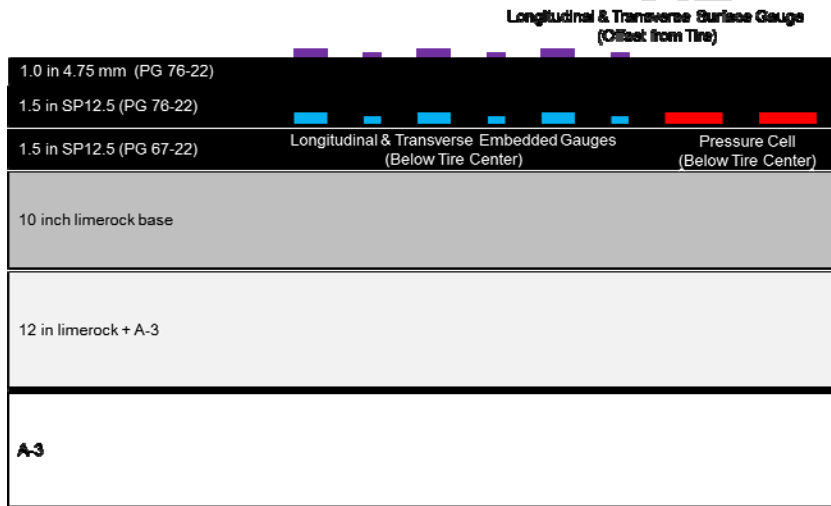
Test Track



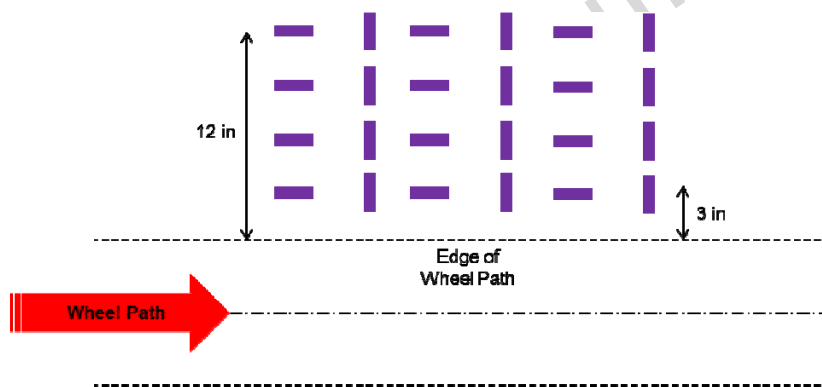
Test Pit Instrumentation



Test Track Instrumentation



Surface Strain Gauges



Instrumentation Summary

Sensor Type	Number of Sensors per Test Section	Model	Vertical Location	Offset from Wheel Path
Surface strain gauge	24	Tokyo Sokki PFL-30-11-5L	HMA surface	Transverse and longitudinal orientations at various offsets from wheel path edge
Asphalt strain gauge	6	Tokyo Sokki KM-100HAS	Bottom of new HMA	Transverse and longitudinal orientations below tire center
Pressure cell	2	RST Instruments LPTPC09-S	Bottom of new HMA	Below tire center
Pressure cell (Test Pit only)	2	Geokon 3500	Bottom of base	Below tire center



Pressure Cells



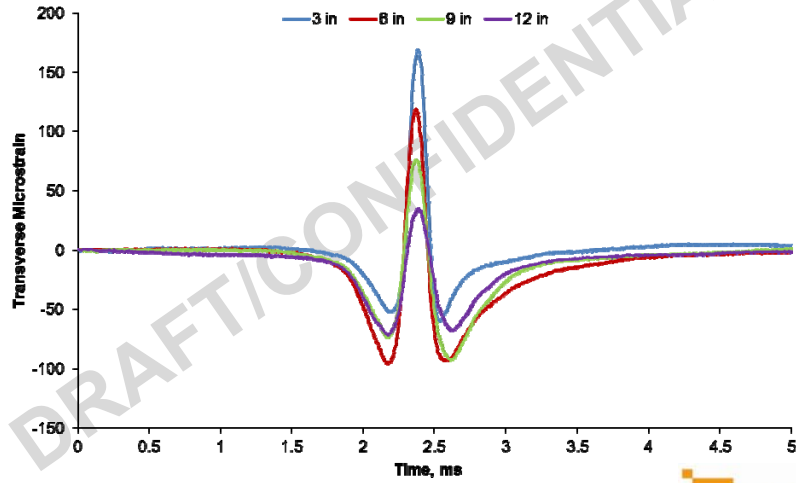
Asphalt Strain Gauges (H-Gauges)



Asphalt Surface Strain Gauges (Foil)



Surface Strain – Dual Tire at 55°C



Test Pit Construction



Test Pit Paving



Test Track Paving



Material Sampling



Laboratory Testing

- Granular Materials
 - Resilient modulus
 - Moisture-density relationship
- HMA
 - Cores
 - Verification of density
 - Cores to University of Illinois
 - Loose mixture
 - Volumetric data
 - IDT
 - AMPT

HVS Test Matrix

Tire Type	Inflation Pressure (psi)	Tire Loading (kips)				
		6	8	10	14	18
NGWB and Dual	80	6	8	10	14	18
NGWB and Dual	100	6	8	10	14	18
NGWB and Dual	110	6	8	10	14	18
NGWB and Dual	125	6	8	10	14	18
Dual Only	60/110	6	8	10	14	18
Dual Only	80/110	6	8	10	14	18

Tests at 25°C, 40°C, and 55°C

Completed Tasks

- The construction, instrumentation, and testing at Florida has been completed

COMMENTS!

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**Instrumentation and Testing:
California**

UC DAVIS
UNIVERSITY OF CALIFORNIA

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Completed Tasks

- HVS response testing on two flexible pavements

- Status: Completed

- Preliminary (CA) for energy (gas) em

- Status



Pavement Structure



Instrumentation

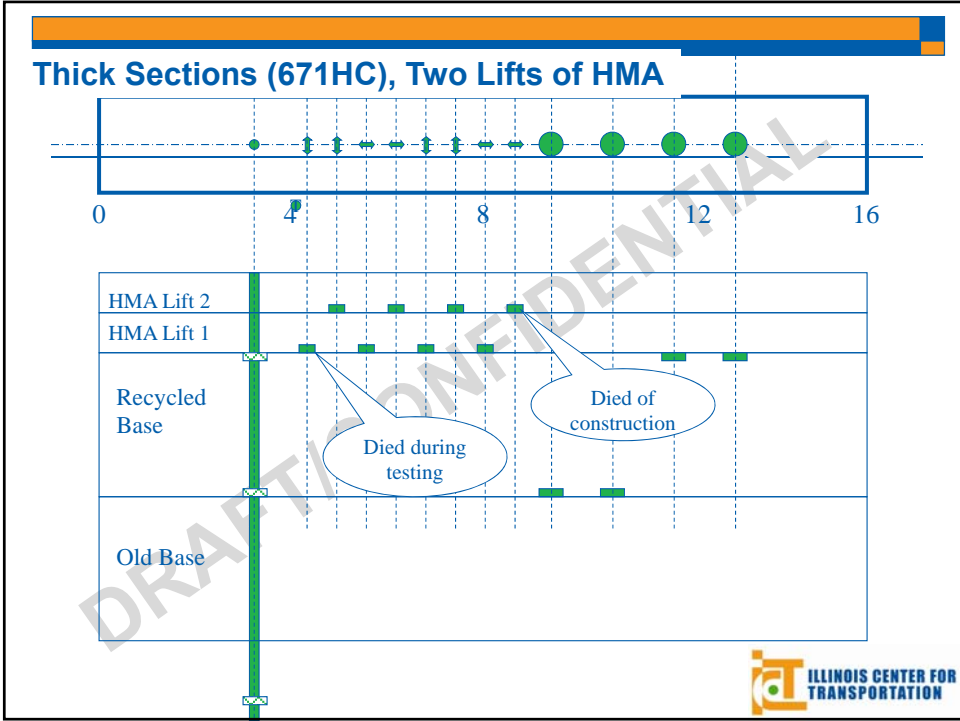
- Strain Gauges
- Pressure Cells
- Multi-Depth Deflectometers
- Thermocouples



Instrumentation

- **Thick Section**
 - 8 Strain Gauges (two malfunctioned, 1 const, 1 testing)
 - 4 Pressure Cells
 - 1 MDD hole with three depths
 - 12 Thermocouples
- **Thin Section**
 - 6 Strain Gauges (two malfunctioned in testing)
 - 1 Pressure Cell
 - 1 MDD hole with four depths
 - 12 Thermocouples

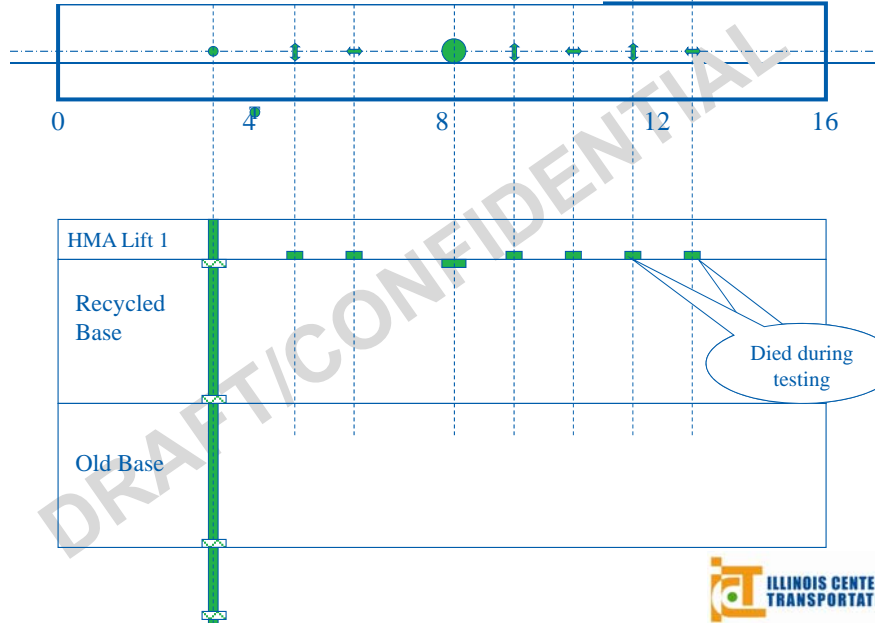




Thick Section Between the Two Lifts of HMA



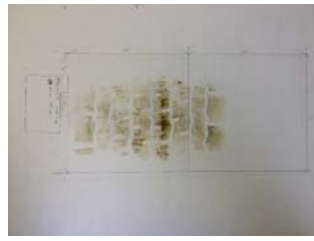
Thick Sections (670HC), One Lift of HMA



Thin Section On Top of the Recycled Aggregate Base



DTA and WBT Imprints



HVS Testing Program – 1/3

- Full Factorial
 - HMA Thickness (2.4 and 4.7 in)
 - Pavement Temperature (69, 95, 122F)
 - Tire Pressure (80,100,110,125 psi for both, 60/110, 80/110 psi for dual)
 - Half Axle Load (6, 8, 10, 14, 18 kips)
- Partial Factorial
 - Lateral Offset (0, 7, 12 in)
- Spot Check (by repetition) in the end



HVS Testing Program – 2/3

- Testing Sequence
 - Perform permutations for half axle loads **less than 18 kips**
 - Wheel type (WBT, DTA)
 - Temperature
 - Tire pressure
 - Load
 - Then repeat with half axle load **at 18 kips**
 - To prevent excessive damage at 18 kips
 - Spot check (repeat selected combinations)
 - Wheel type
 - Temperature
 - Tire pressure



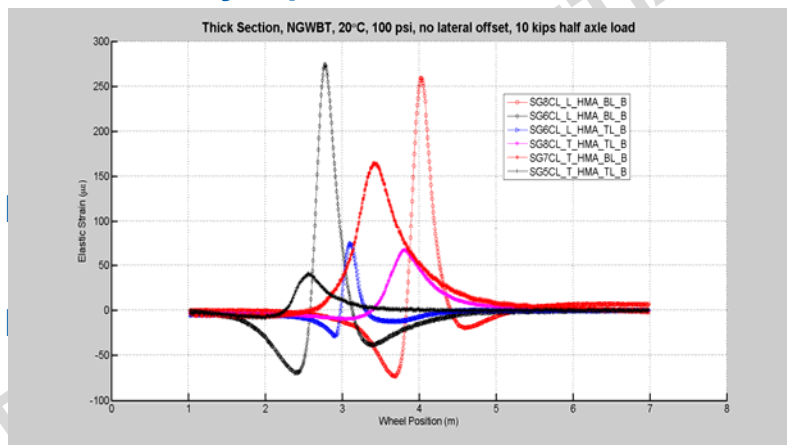
HVS Testing Program 3/3

- **174** combinations in total
- **Each combination:**
 - 100 repetitions
 - Constant speed of 8 km/h
 - Channelized (no wander)
- **Thick Section**
 - 3/6/2013~4/15/2013
 - 22,100 repetitions total
- **Thin Section**
 - 4/26/2013~5/20/2013
 - 20,300 repetitions total



Data Collection

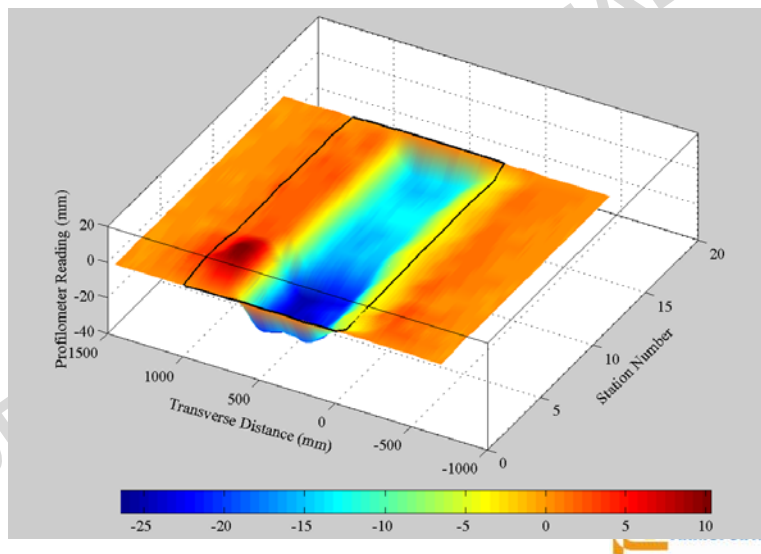
- **Record every repetition:**



After HVS Testing – Thin Section



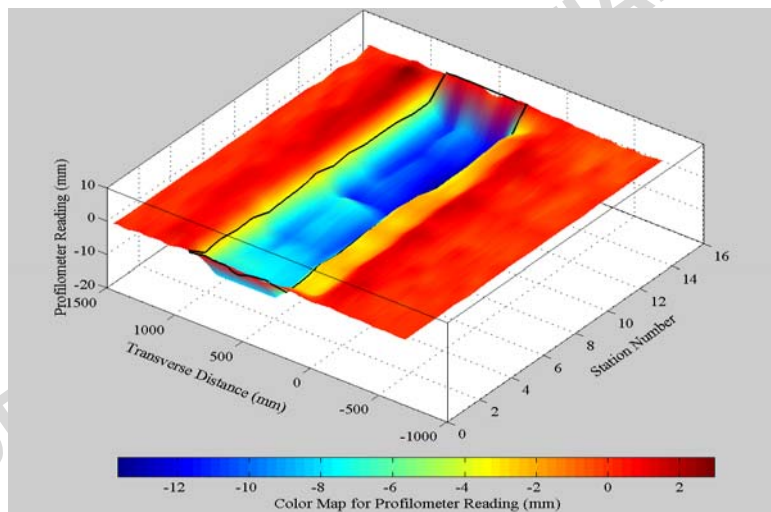
Surface Rut Contour – Thin Section



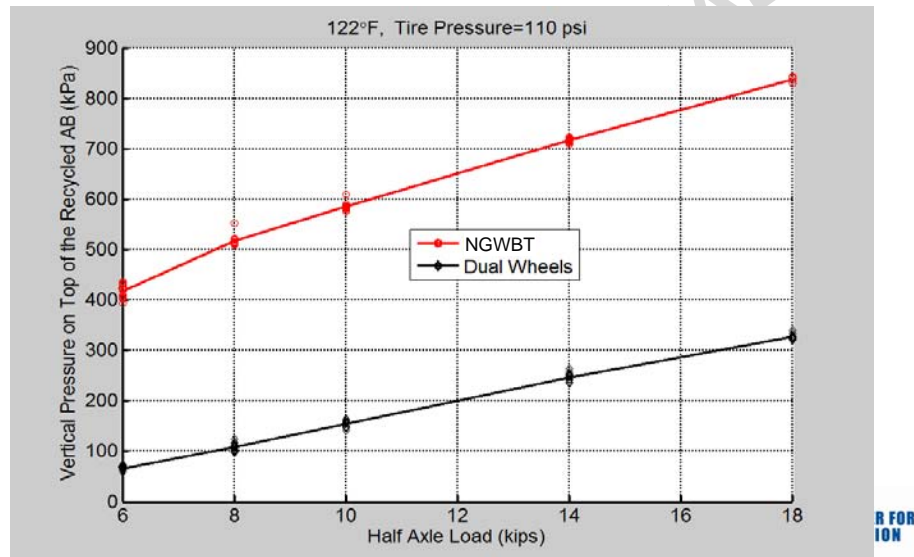
After HVS Testing – Thick Section



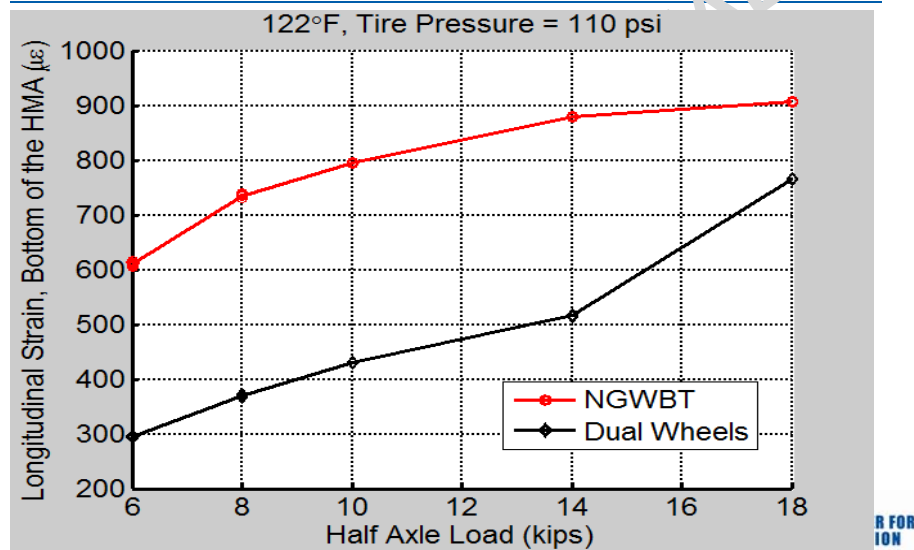
Surface Rut Contour – Thick Section



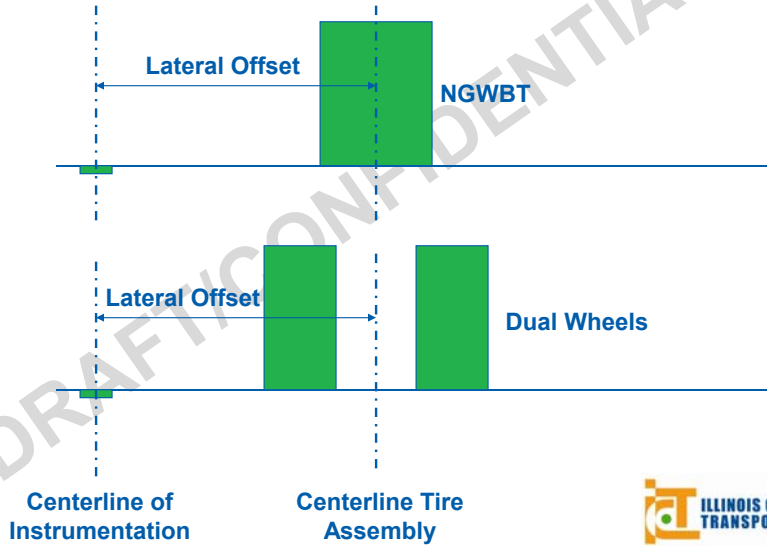
Example of Preliminary Results – Thin Section, Vertical Pressure at Bottom of the HMA



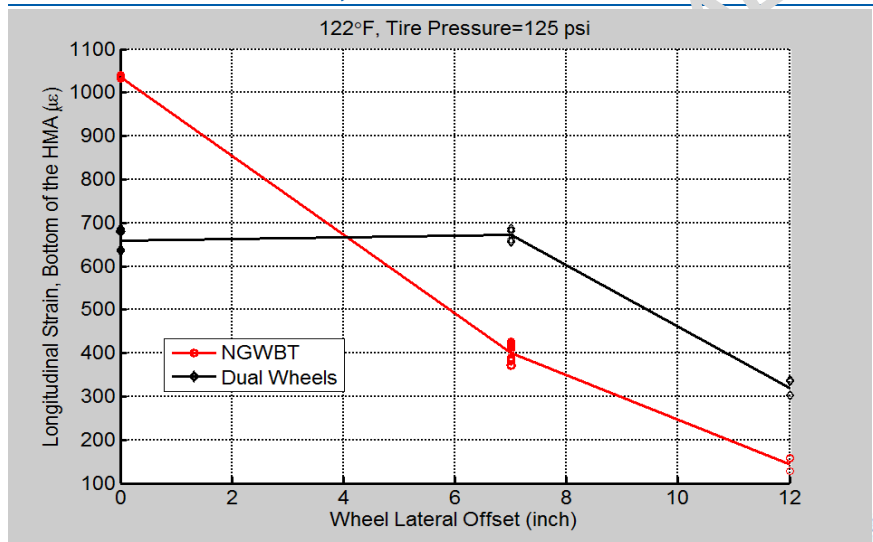
Example of Preliminary Results – Thin Section, Longitudinal Strain at Bottom of HMA (First Lift)



Definition of Lateral Offset



Preliminary Results – Strain in Thick Section, Effect of Lateral Offset

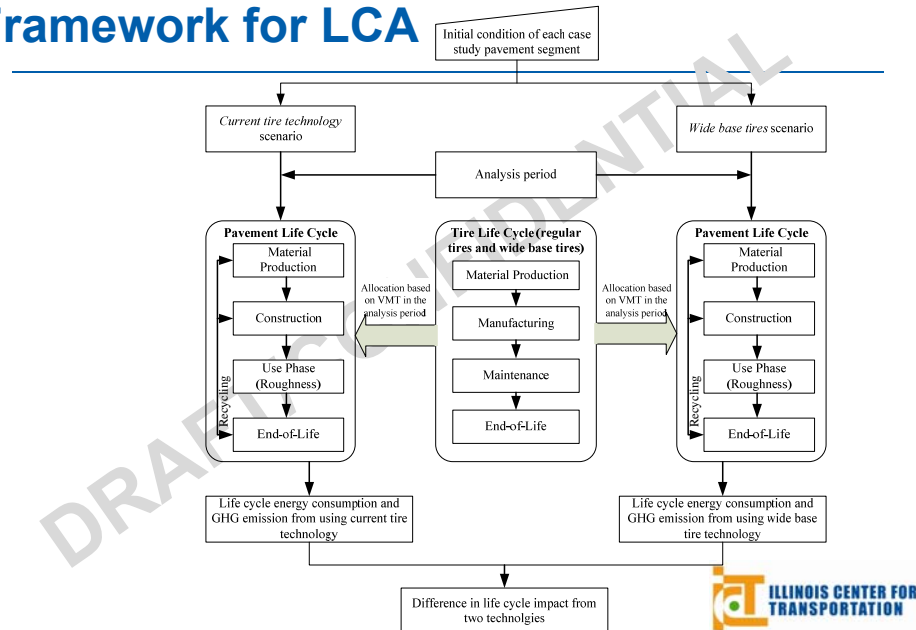


LCA - Basic Approach

- Select scenarios for pavement network based on:
 - Traffic level
 - Pavement Structure
- For each scenario perform LCA
 - Using existing inventories
- Additional sensitivity analyses on:
 - Market penetration rates, types, traffic levels, congestion levels, etc.
- Deliverables:
 - Framework for LCA
 - Provide guidance for decision makers on impact of NGWBT
 - Suggest particular scenarios where impact is greater



Framework for LCA



Remarks

- Significant **difference** in pavement **responses** between **Dual** and **NGWBT** were observed.
- Testing caused **rutting** in the pavement, which did not affect the relative comparison.
- Effect of wheel **lateral offset** needs to be considered when making comparisons.
- **LCA framework** established, will need some inputs to the model.





Future Plans

- Complete APT test matrix
- Data collection for life-cycle inventory
- LCA case studies



COMMENTS!



**Instrumentation and Testing:
Ohio**



Outline

- Project description
- Typical section
- Instrumentation
- Material sampling
- Controlled loading test

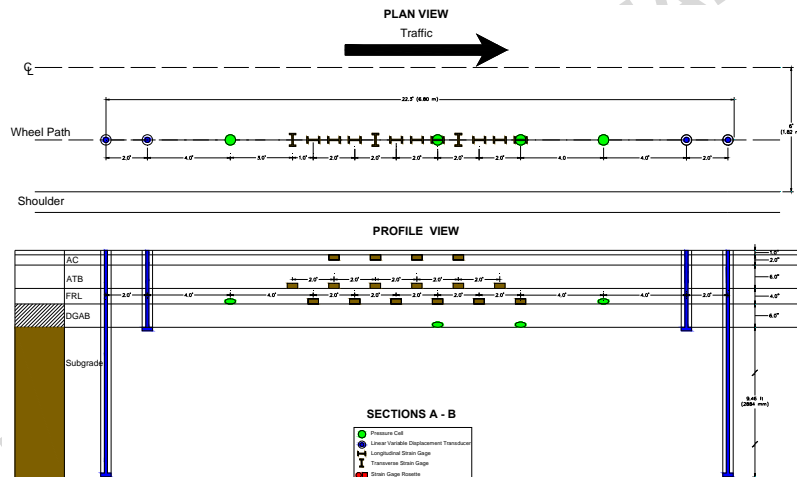


Project Description

- Located in **Delaware, OH** (US-23)
- Optimization of AC thickness in perpetual pavements
- Three **heavily instrumented** pavement sections (AC thickness: 13 and 15 in)
- Truck load test: WBT and DTA; single and tandem axle



Typical Section



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Instrumentation

- ❑ Deep and shallow **LVDTs**
- ❑ **Pressure cells** at the bottom of AC and base
- ❑ **Thermocouples**
- ❑ **Strain gauges** in longitudinal and transverse directions at various depths
- ❑ **Rosettes** strain gauges



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Pressure Cells

Pressure cells on top of subgrade



Pressure cells on top of DGAB



Strain Gauges



Strain Gauges Rosettes



Material sampling

Loose mix from each material (layer)



Material sampling

Compacted samples from each material (layer)



Controlled Truck Loading Test

Tire load (kip)	Speed (mph)	Tire pressure (psi)	Tire configuration	Axle Configuration
10, 14	5, 30, and 55	80, 110, 125	WBT-445 & DTA-275	Single & Tandem



Controlled Truck Loading Test



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Controlled Truck Loading Test



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COMMENTS!


DRAFT/CONFIDENTIAL



Future Plans Discussion
3:30-3:45pm

5/30/2013

DRAFT/CONFIDENTIAL



Future Plans

- **Contact stresses**
 - Complete detailed contact stress analysis of DTA and WBT magnitude and distribution
 - Prediction of contact stresses using FEM
- **Modeling**
 - Complete thin and thick pavement cases with various combinations of axle loads and tire inflation pressures
 - Provide a analysis considering the effect of tire type; material property; loading characteristics; and pavement structure



Future Plans

- **Laboratory testing:**
 - Compact SGC specimens that simulate field-compacted samples (air void validation)
 - Complete laboratory test matrix for materials in all testing sites
- **Complete APT and field-instrumented data collection and analysis**
- **Finalize the instrumentation response database**
- **Preliminary LCA scenarios**
- **Marketing and publications**



COMMENTS!



**Technical Committee
Discussion**
3:45-4:15pm

5/30/2013



COMMENTS!

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Final Remarks
4:15-4:45pm

5/30/2013

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