Transportation Pooled Fund Program TPF-5(446) Quarterly Progress Report

Quarter 3, July – September 2023

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TRANSPORTATION POOLED FUND PROGRAM
QUARTERLY PROGRESS REPORT

Lead Agency (FHWA or State DOT): _FHWA_______________________________________

INSTRUCTIONS:
Project Managers and/or research project investigators should complete a quarterly progress report for each calendar quarter during which the projects are active. Please provide a project schedule status of the research activities tied to each task that is defined in the proposal; a percentage completion of each task; a concise discussion (2 or 3 sentences) of the status, including accomplishments and problems encountered, if any. List all tasks, even if no work was done during this period.

Transportation Pooled Fund Program Project # *(i.e., SPR-2(XXX), SPR-3(XXX) or TPF-5(XXX)*	**Transportation Pooled Fund Program - Report Period:**
TPF-5(446)	☐Quarter 1 (January 1 – March 31) ☐Quarter 2 (April 1 – June 30) ☒Quarter 3 (July 1 – September 30) ☐Quarter 4 (October 1 – December 31)

Project Title:
High Performance Computational Fluid Dynamics (CFD) Modeling Services for Highway Hydraulics

Name of Project Manager(s):	**Phone Number:**	**E-Mail**
Kornel Kerenyi	*(202) 493-3142*	*kornel.kerenyi@fhwa.dot.gov*
Lead Agency Project ID:	**Other Project ID (i.e., contract #):**	**Project Start Date:**
Original Project End Date:	**Current Project End Date:**	**Number of Extensions:**

Project schedule status:

☒ On schedule ☐ On revised schedule ☐ Ahead of schedule ☐ Behind schedule

Overall Project Statistics:

Total Project Budget	Total Cost to Date for Project	Percentage of Work Completed to Date

Quarterly Project Statistics:

Total Project Expenses and Percentage This Quarter	Total Amount of Funds Expended This Quarter	Total Percentage of Time Used to Date

Project Description:

The Federal Highway Administration established an Inter-Agency Agreement (IAA) with the Department of Energy's (DOE) Argonne National Laboratory (ANL) Transportation Analysis Research Computing Center (TRACC) to get access and support for High Performance Computational Fluid Dynamics (CFD) modeling for highway hydraulics research conducted at the Turner-Fairbank Highway Research Center (TFHRC) Hydraulics Laboratory. TRACC was established in October 2006 to serve as a high-performance computing center for use by U.S. Department of Transportation (USDOT) research teams, including those from Argonne and their university partners. The objective of this cooperative project is to:

- Provide research and analysis for a variety of highway hydraulics projects managed or coordinated by State DOTs.
- Provide and maintain a high-performance Computational Fluid Dynamics (CFD) computing environment for application to highway hydraulics infrastructure and related projects.
- Support and seek to broaden the use of CFD among State Department of Transportation employees.

The work includes:

- Computational Mechanics Research on a Variety of Projects: The TRACC scientific staff in the computational mechanics focus area will perform research, analysis, and parametric computations as required for projects managed or coordinated by State DOTs.
- Computational Mechanics Research Support: The TRACC support team consisting of highly qualified engineers in the CFD focus areas will provide guidance to users of CFD software on an as needed or periodic basis determined by the State DOTs.
- Computing Support: The TRACC team will use the TRACC clusters for work done on projects; The TRACC system administrator will maintain the clusters and work closely with the Argonne system administrator's community; The TRACC system administrator will also install the latest versions of the STAR-CCM+ and OpenFOAM CFD software and other software that may be required for accomplishing projects.

Progress this Quarter:

(Includes meetings, work plan status, contract status, significant progress, etc.)

1: Computational Mechanics Research on a Variety of Projects

1.1: Hydraulic Efficiency of Michigan DOT Cover 'C' in on-Grade and Sag Locations

The hydraulic performance of the catch basin cover 'C' has been analyzed for on-grade and sag locations with the use of computational fluid dynamics software STAR-CCM+ v.17.06. The Michigan DOT engineers use the cover on freeways with 8 to 10-feet-wide shoulders at 4% and traveled lanes usually sloped at 2%, among others. The longitudinal grade varies between 0.3% and 5%. The maximum flow rate used in the analysis is about 2 cfs.

The cover is composed of a grate and a curb box and is for use with a concrete curb and gutter. Figure 1 shows drawings of the cross section of the gutter, cover C assembly, and a plan view of the grate.

(a) (b) (c)

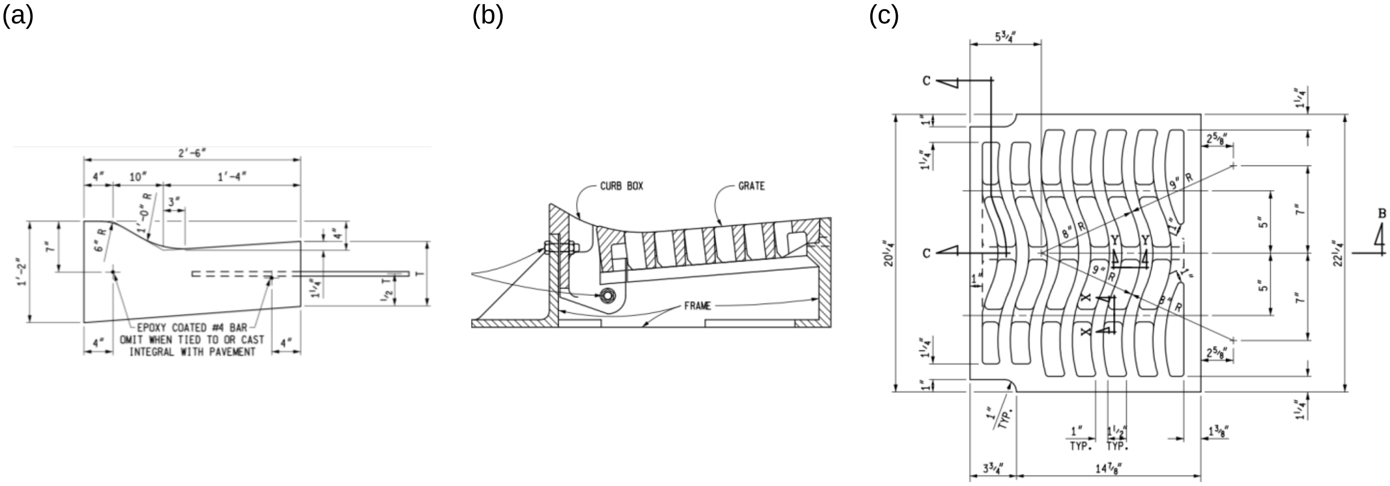

Figure 1. Standard drawings

The computational domain for the on-grade condition is shown in Figure 2. It covers a section of a roadway pavement, curb and gutter and the cover C with a catch basin underneath. The geometry was recreated based on the standard drawings provided by MDOT.

The open-channel flow on pavement is simulated with Eulerian multiphase model to account for phase 1: water and phase 2: air. Volume of fluid model is used to find the interface between the phases i.e., water surface. Surface tension force on the interface between the two phases is also defined. The selected flow solver is unsteady RANS with SST k-ω turbulence model and wall functions with roughness height to model turbulent flow on a rough surface. The cross- slope is represented in the geometry of the pavement, and the longitudinal slope is modeled by modification of the components of the gravitational acceleration vector.

Different boundary conditions on the model surfaces are marked with different colors in Figure 2. The color coding is as follows: orange – pressure outlet with atmospheric pressure, red – inlet velocity, grey – rough wall boundary. Figure 3 shows an example velocity distribution at the inlet to the computational domain. Firstly, the mean velocity and spread are calculated using the Manning formula for the combination of cross – and longitudinal slope, and discharge. Then, the fully-developed velocity distribution is computed using an additional computational model that simulates a small section of a long road by employing the periodic translational boundary conditions with an assumed mass flow rate. Finally, the obtained velocity magnitude and phase (water and air) distribution is used as the inlet conditions in the main model.

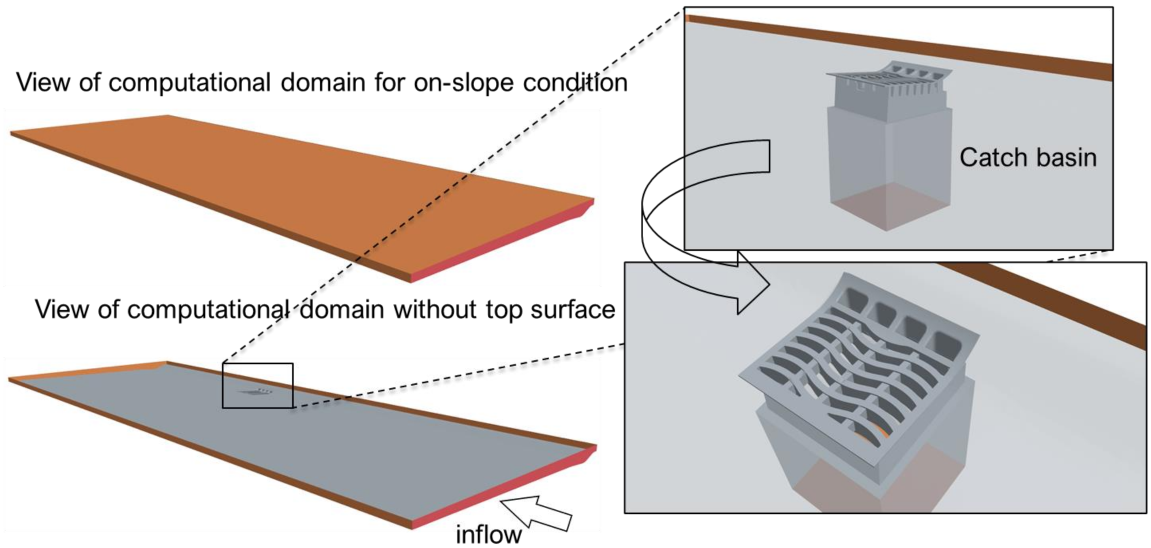

Figure 2. Computational domain for on-slope condition

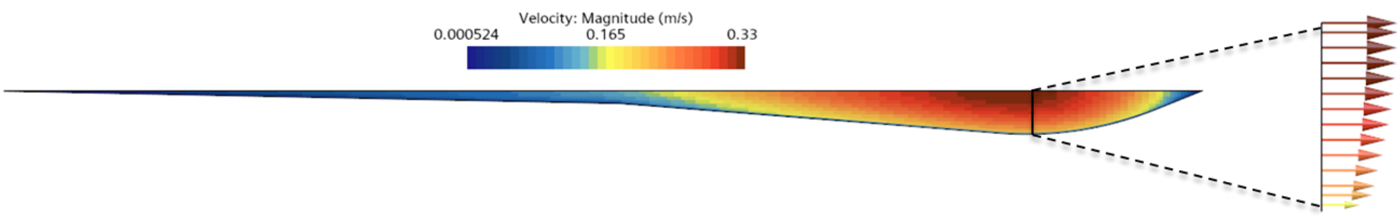

Figure 3. Example of fully developed velocity distribution

The Manning coefficient used by MDOT is typically 0.020 to account for drainage efficiency losses due to pavement roughness, but also debris, such as dry leaves, grass clippings, trash, etc., that accumulate in the vicinity of the drainage. In the computational model, the roughness of the pavement is taken into account with the use of the rough wall functions with a roughness height corresponding to Manning coefficient 0.016 and the clogging of the grate is modeled by closing the orifices of the grate in varying percentage. The conversion from Manning's 'n' and roughness height is done using the Colebrook-White equation as presented in [1, 2].

Project deliverables cover: the hydraulic efficiency as a ratio of intercepted to total flow on a grade, and orifice and weir flow regime, and transition between them in sump condition, among others. The following figures present some of the current findings.

The impact of debris clogging the grate on the flow interception is shown on an example geometry and flow conditions of longitudinal grade 0.01 ft/ft and upstream flow spread 4 ft. The flow pattern in the case of an unobstructed grate is shown on the left in Figure 4. The debris e.g., a pile of dry leaves, grass clippings etc., was modeled as a cylindrical shape blocking 25% of the grate openings. The addition of this obstruction results in wider spread of the flow around the grate, an increase in flow bypassing it, and therefore lower interception; the hydraulic efficiency drops from 85% to 72%. Figure 4 (right) shows the flow on the pavement in these conditions.

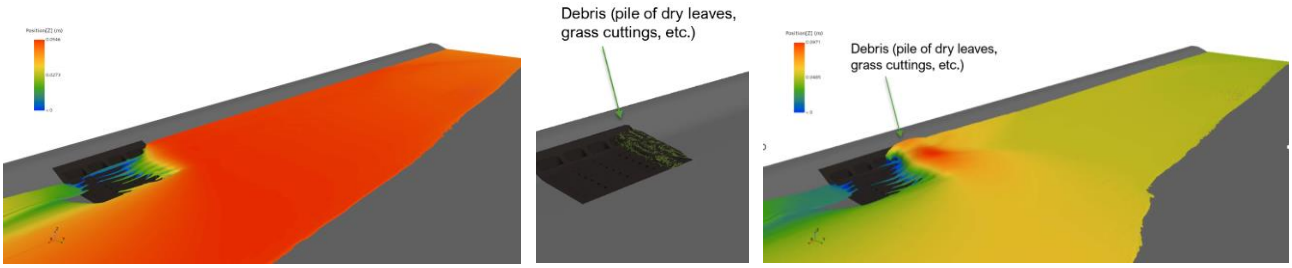

Figure 4. Comparison of flow pattern for an unobstructed (left) and partially clogged (right) grate, for example conditions of longitudinal grade 0.01 ft/ft and upstream flow spread 4 ft.

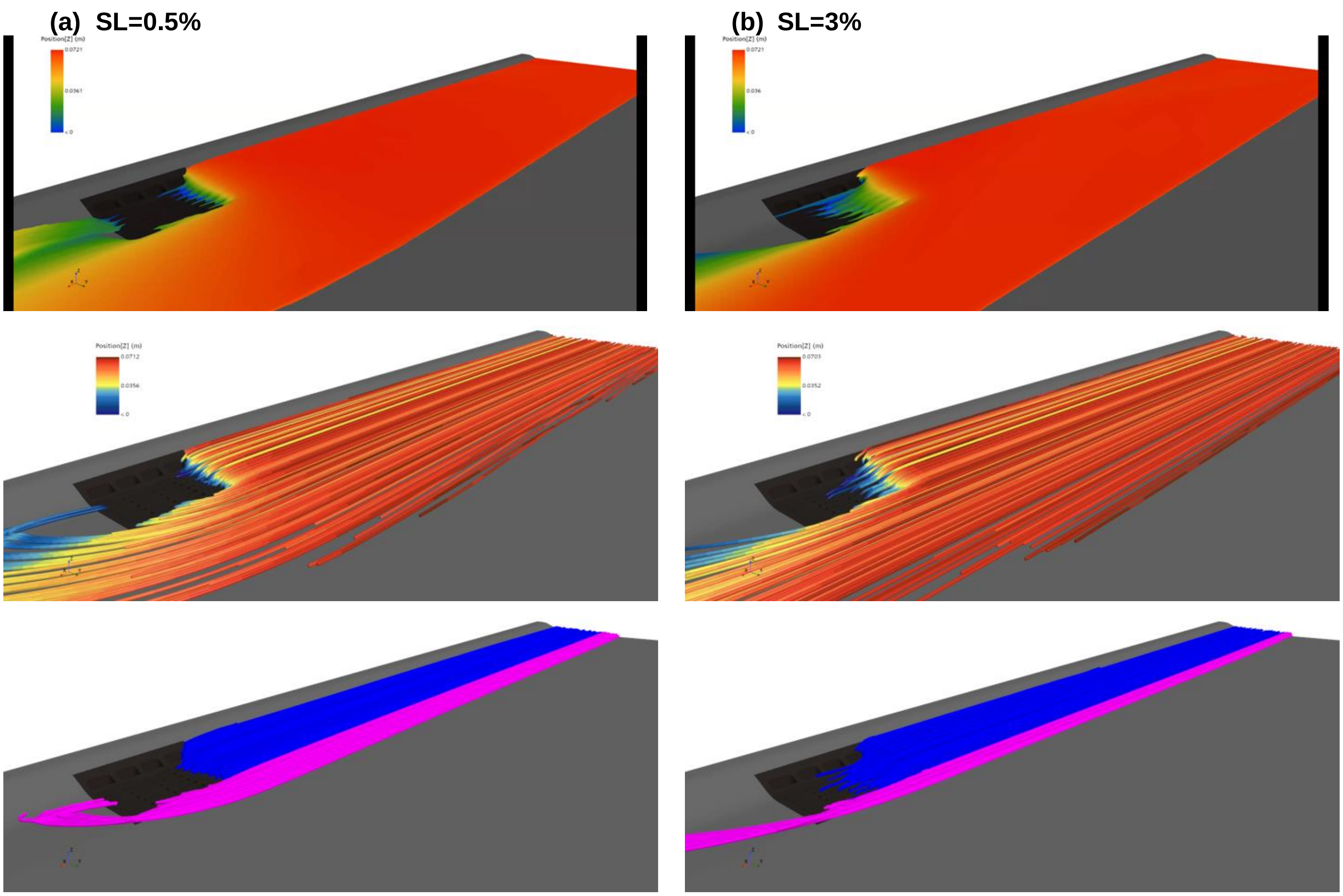

Figure 5. Influence of the longitudinal grade on the flow interception. Example: upstream spread 5 ft, longitudinal grade (a) 0.5%, and (b) 3%. Top: water surface, center: velocity streamlines, bottom: streamlines intercepted by the front of the grate (blue) and intercepted by the side of the grate (pink).

The front and side interception of the grate depends on various factors, like discharge, cross- and longitudinal slope, among others. Figure 5 shows an example of a flow on the pavement that is 5-feet-wide upstream of the grate at two longitudinal slopes (a) 0.5%, and (b) 3%. On top of the figure, the water surface is shown, in the center: the velocity streamlines, and on the bottom: the streamlines intercepted by the front of the grate (blue) and those intercepted by the side of the grate (pink). Firstly, the increase in slope results in an increase of the portion of the flow that bypasses the grate. At SL=0.5%, a small portion of the flow bypasses the side of the grate but is intercepted by its back side. This backflow is not seen in the case of SL=3%. Secondly, at smaller longitudinal slopes, the flow is mostly intercepted by the edge openings of the grate; at increased slope, a greater percentage of the grate takes part in the flow interception. Thirdly, in both cases the frontal flow (the part of the upstream gutter flow within the width of the grate) is fully intercepted, but the side flow decreases with an increase in the longitudinal slope.

The analysis of the Michigan DOT Cover 'C' will continue with the focus on the sag locations. The influence of clogging on the ponding depth at varying discharge will be analyzed, among others.

References:
[1] Sitek, M.A. and S.A. Lottes. "Computational Analysis of Water Film Thickness During Rain Events for Assessing Hydroplaning Risk Part 2: Rough Road Surfaces.", Argonne National Laboratory, ANL-20/37, July 2020.
[2] M.A. Sitek, S.A. Lottes, J. Syar, Computational Analysis of Hydraulic Capacity of Ohio DOT Catch Basins On-Grade and in Sag Locations, ANL-21/20, April 2021

Anticipated work next quarter:

1: Computational Mechanics Research on a Variety of Projects

- hydraulic analysis of catch basins on grade and in sump
- analysis of water film thickness on pavements (hydroplaning water film thickness and speed)

2: Computational Mechanics Research Support

This work will continue.

Task 3: Computing Support

This work will continue.

Circumstance affecting project or budget.

(Please describe any challenges encountered or anticipated that might affect the completion of the project within the time, and fiscal constraints set forth in the agreement, along with recommended solutions to those problems).

None.